

116. Measurement of longitudinal vibrations of the rollers in a folding machine

E. Kibirškis¹, V. Miliūnas², S. Havenko³, K. Ragulskis⁴, L. Ragulskis⁵

^{1,2}Kaunas University of Technology, Department of Manufacturing Engineering, Studentų 56-350, LT-51424, Kaunas, Lithuania

³Ukrainian Academy of Printing, Podgolosko 19, 79020, Lviv, Ukraine

⁴Kaunas University of Technology, Kaunas, 44029, Lithuania

⁵Vytautas Magnus University, Kaunas, 44404, Lithuania

¹Corresponding author

E-mail: ¹edmundas.kibirsktis@ktu.lt, ²valdas.miliunas@ktu.lt, ³havenko@point.lviv.ua,

⁴kazimieras3@hotmail.com, ⁵l.ragulskis@if.vdu.lt

Received 20 January 2017; received in revised form 10 March 2017; accepted 23 March 2017

DOI <https://doi.org/10.21595/jme.2017.18375>



Abstract. In paper folding machines vibrations of rollers and of their segments take place. Thus, it is important to perform measurements of those vibrations and to investigate vibrational processes in those rollers. Measurements are performed by using a laser displacement head of the type “Microtrack LTC 200-100”. Specific positions of rollers and of their segments were pre-selected. Measurements were performed at those positions and the obtained results were processed and investigated. Vibrational effects taking place in rollers and also in their segments during the process of rotation influence the quality of produced printing materials. Plane strain problem is investigated and supplementary stiffness from the static loading caused by centrifugal forces is taken into account. Eigenmodes of longitudinal vibrations are investigated.

Keywords: experimental setup, measurement of vibrations, folding machine, quality of printing, roller, rotating element, printing products, plane strain, centrifugal forces, longitudinal vibrations, eigenmodes.

1. Introduction

In paper folding machines vibrations of rollers and of their segments take place. Thus, it is important to perform measurements of those vibrations and to investigate vibrational processes in those rollers. Measurements are performed by using a laser displacement head of the type “Microtrack LTC 200-100”. Specific positions of rollers and of their segments were pre-selected. Measurements were performed at those positions and the obtained results were processed and investigated. Vibrational effects taking place in rollers and also in their segments during the process of rotation influence the quality of produced printing materials.

Plane strain problem is investigated and supplementary stiffness from the static loading caused by centrifugal forces is taken into account. Eigenmodes of longitudinal vibrations are investigated.

This paper is a continuation of previous investigations which were presented in [1, 2]. Process of experimental investigations is performed and the experimental setup was implemented on the basis of material described in [3-6]. The numerical procedure is based on the material described in the earlier papers as well as presented in [7-10]. Problems of similar character were also analyzed in a number of other papers [11-21].

Thus, the aim of this paper is to determine the level of wear of rollers located in the folding machine by measuring the surface displacements of rollers.

2. Numerical model for the analysis of longitudinal vibrations of a rotating structure

Further x and y denote the axes of the system of coordinates. The stiffness matrix of the plane strain problem has the usual form:

$$[K] = \int [B]^T [D] [B] dx dy, \quad (1)$$

where:

$$[B] = \begin{bmatrix} \frac{\partial N_1}{\partial x} & 0 & \dots \\ 0 & \frac{\partial N_1}{\partial y} & \dots \\ \frac{\partial N_1}{\partial y} & \frac{\partial N_1}{\partial x} & \dots \end{bmatrix}, \quad (2)$$

where N_1, N_2, \dots, N_9 are the shape functions of the finite element. In the investigation two dimensional Lagrange quadratic element is used. The matrix of elastic constants has the usual form:

$$[D] = \begin{bmatrix} K + \frac{4}{3}G & K - \frac{2}{3}G & 0 \\ K - \frac{2}{3}G & K + \frac{4}{3}G & 0 \\ 0 & 0 & G \end{bmatrix}, \quad (3)$$

where:

$$K = \frac{E}{3(1 - 2\nu)}, \quad (4)$$

$$G = \frac{E}{2(1 + \nu)}, \quad (5)$$

where E is modulus of elasticity and ν is Poisson's ratio.

The loading vector of centrifugal forces for the investigated plane strain problem corresponding to the angular velocity $\omega = 1$ rad/sec has the following form:

$$\{F\} = \int [N]^T \begin{Bmatrix} \rho x \\ \rho y \end{Bmatrix} dx dy, \quad (6)$$

where ρ is the density of material of the analyzed structure. The matrix of shape functions has the usual form:

$$[N] = \begin{bmatrix} N_1 & 0 & \dots \\ 0 & N_1 & \dots \end{bmatrix}. \quad (7)$$

By solving the static problem for the previously described loading by centrifugal forces the vector of nodal displacements $\{\delta\}$ is determined in the conventional way.

The total stiffness matrix for longitudinal motion which corresponds to rotation of the structure by the angular velocity ω is of the following form:

$$[\bar{\bar{K}}] = [\bar{K}] + \omega^2 [K_\sigma]. \quad (8)$$

The stiffness matrix for longitudinal motion of the plane strain problem has the following form:

$$[\bar{K}] = \int [\bar{B}]^T [\bar{D}] [\bar{B}] dx dy, \quad (9)$$

where:

$$[\bar{B}] = \begin{bmatrix} \frac{\partial N_1}{\partial y} & \dots \\ \frac{\partial N_1}{\partial x} & \dots \end{bmatrix}, \quad (10)$$

and the matrix of elastic constants has the following form:

$$[\bar{D}] = \begin{bmatrix} G & 0 \\ 0 & G \end{bmatrix}. \quad (11)$$

The supplementary stiffness matrix for longitudinal motion caused by centrifugal loading has the following form:

$$[K_\sigma] = \int [G]^T [M_\sigma] [G] dx dy, \quad (12)$$

where:

$$[G] = \begin{bmatrix} \frac{\partial N_1}{\partial x} & \dots \\ \frac{\partial N_1}{\partial y} & \dots \end{bmatrix}, \quad (13)$$

and:

$$[M_\sigma] = \begin{bmatrix} \sigma_x & \tau_{xy} \\ \tau_{xy} & \sigma_y \end{bmatrix}. \quad (14)$$

The stresses caused by centrifugal loading in the latter expression are determined from the following relationship:

$$\begin{Bmatrix} \sigma_x \\ \sigma_y \\ \tau_{xy} \end{Bmatrix} = [D][B]\{\delta\}. \quad (15)$$

The mass matrix for longitudinal motion has the following form:

$$[M] = \int [\bar{N}]^T \rho [\bar{N}] dx dy, \quad (16)$$

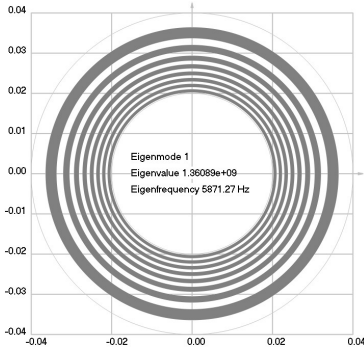
where:

$$[\bar{N}] = [N_1 \quad \dots]. \quad (17)$$

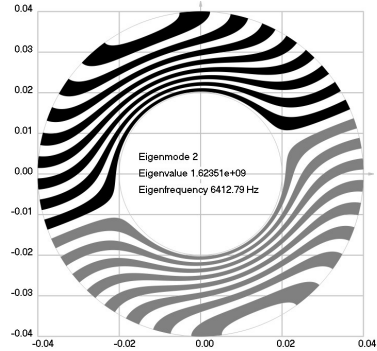
3. Eigenmodes of longitudinal vibrations of the rotating element of the folding machine

The geometry of the investigated structure is a circle having internal radius 0.02 m and external radius 0.04 m. It is assumed that all nodal displacements are equal to zero on the internal radius of the circle. The following parameters of the analyzed structure are assumed: modulus of

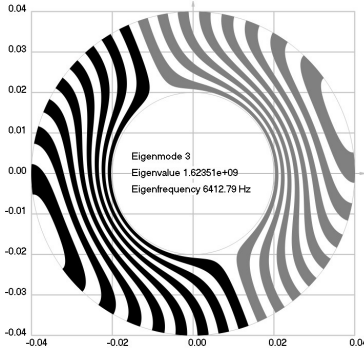
elasticity $E = 6 \times 10^8$ Pa, Poisson's ratio $\nu = 0.3$, density of the material of the investigated structure $\rho = 785 \text{ kg/m}^3$.



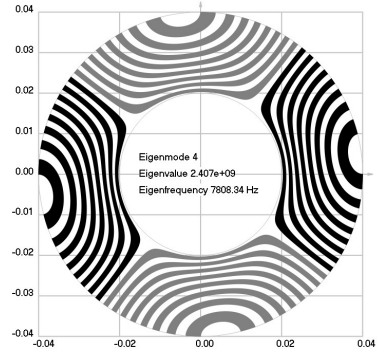
a)



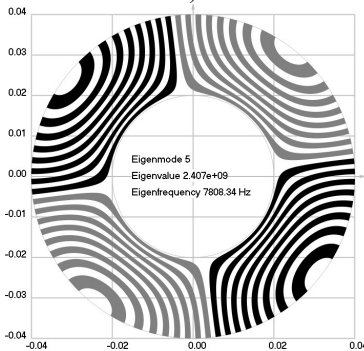
b)



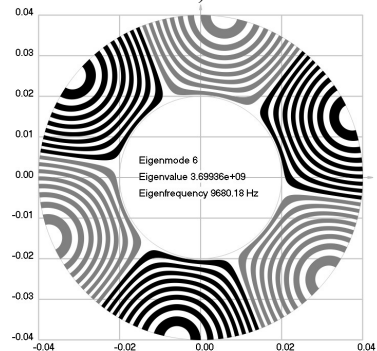
c)



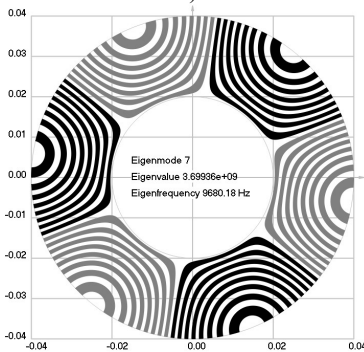
d)



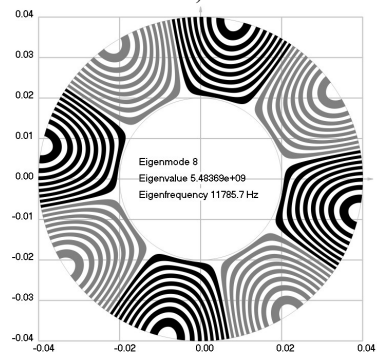
e)



f)



g)



h)

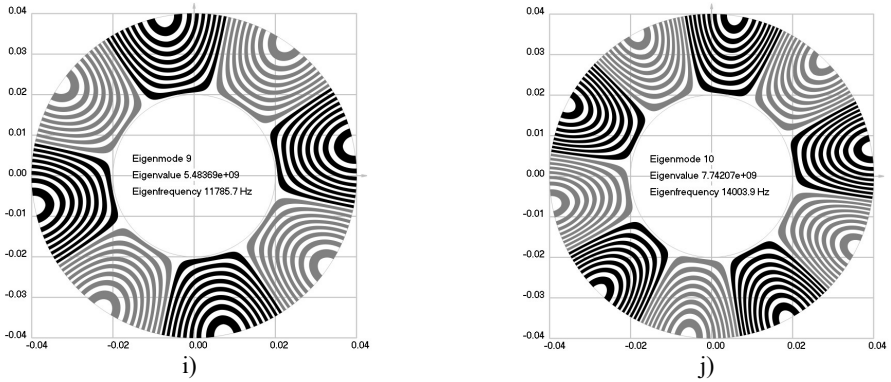
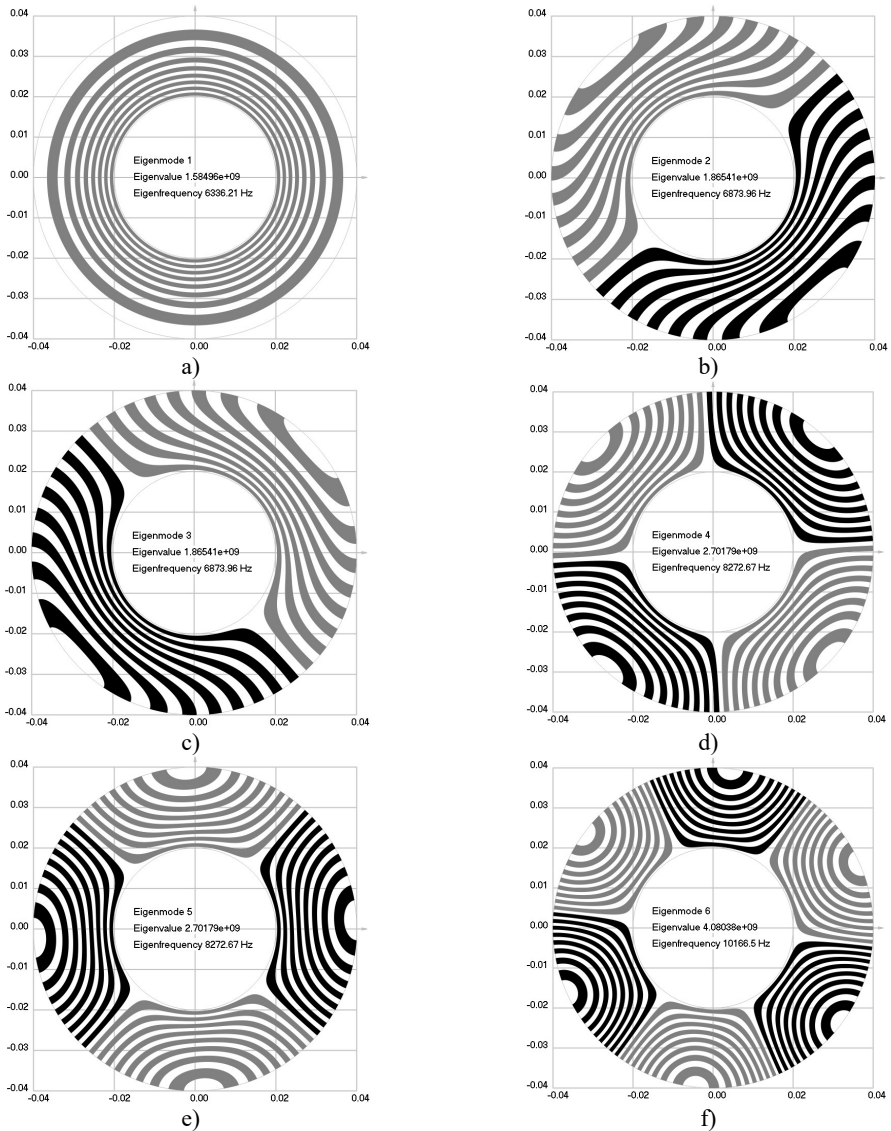


Fig. 1. Eigenmodes of longitudinal motion when the investigated structure does not rotate: a) the first eigenmode, b) the second eigenmode, ..., j) the tenth eigenmode



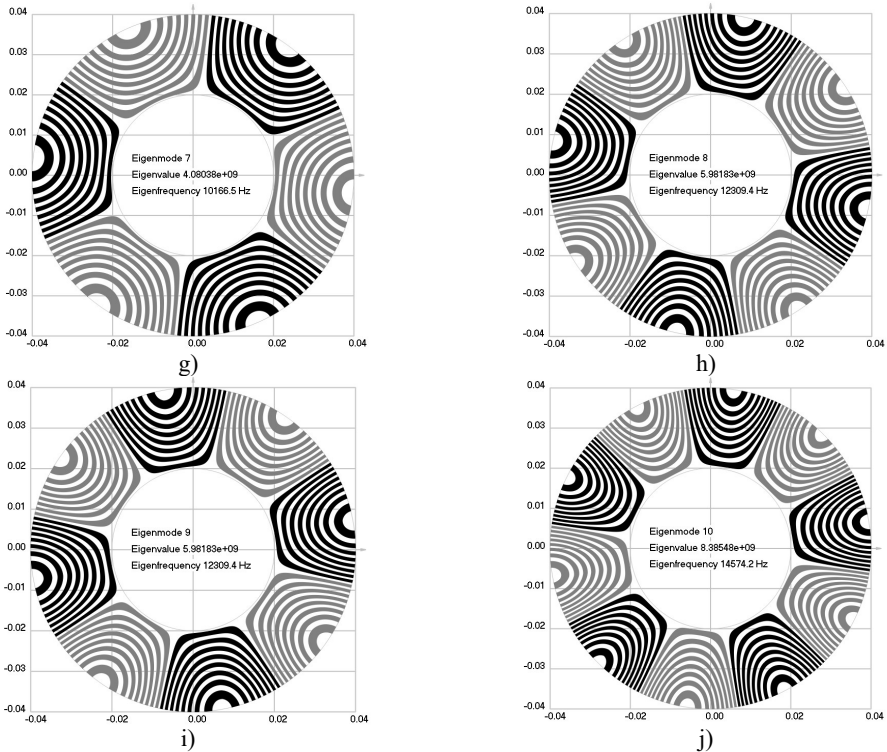


Fig. 2. Eigenmodes of longitudinal motion when the investigated structure rotates:
 a) the first eigenmode, b) the second eigenmode, ..., j) the tenth eigenmode

The first ten eigenmodes of longitudinal motion for $\omega = 0$ rad/sec are shown in Fig. 1.

The first ten eigenmodes of longitudinal motion for $\omega = \sqrt{10^8}$ rad/sec are shown in Fig. 2.

From the presented results, the effect of supplementary stiffness because of the stresses caused by centrifugal forces to the eigenfrequencies of the analyzed structure is clearly seen.

4. Results of experimental investigations of dynamics of rollers

Laser head “Microtrack LTC 200-100” was used in the performed investigation. Dynamic processes of rollers and of their segments were measured by using this laser head. The simplest method to make the rollers rotate in the process of experimental investigation is to rotate them manually. So, in the performed investigation this approach was adopted. Data of performed measurements were transferred to the personal computer. Planning the experimental investigation involved the pre-selection of a number of points in which measurements were performed (see Fig. 3). The selection of measurement points and their locations were described in the previous papers of the authors. Low frequency filter was used in order to make the results of experimental investigations interpretable. In the earlier papers the authors did present the material related with the design of the proposed experimental setup and the process of experimental investigations in detail.

Some of the obtained typical results from the performed measurements of displacements at pre-selected points of the rollers are presented in Fig. 4.

Dynamical processes of complicated character are obtained as a result of performed measurements. The designed low pass digital filter after applying appropriate values of the parameters enables to obtain satisfactory correspondence with the results represented by the eigenmodes obtained numerically.

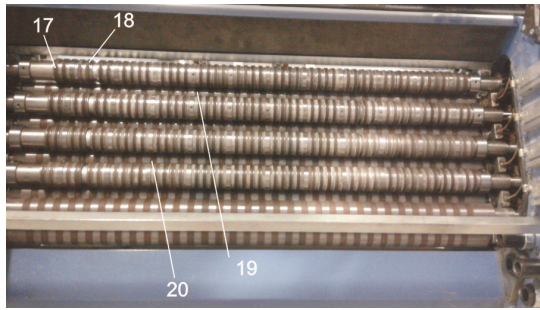
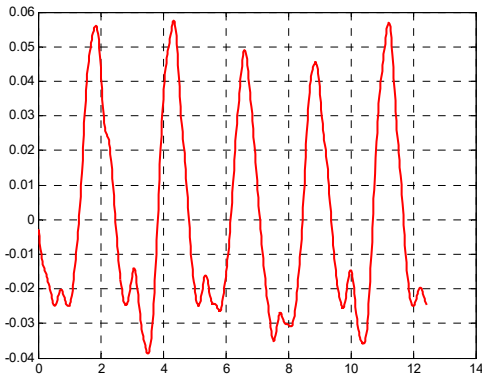
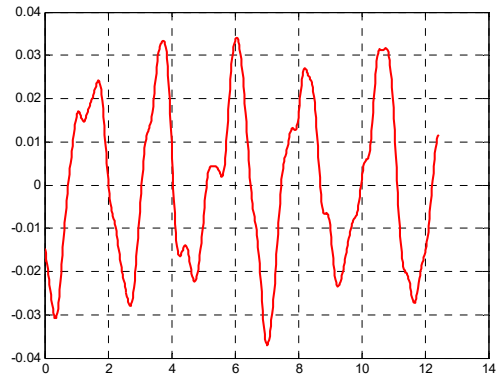


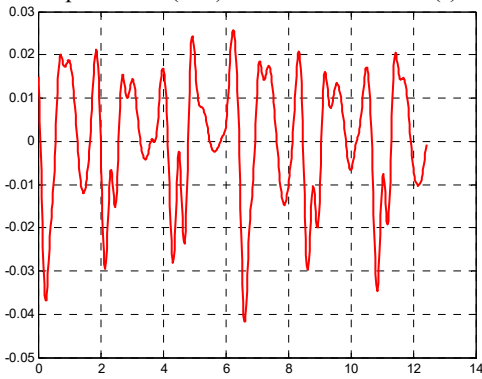
Fig. 3. External view of 8 pockets of the folding machine and of the pre-selected points of measurements (17-20)



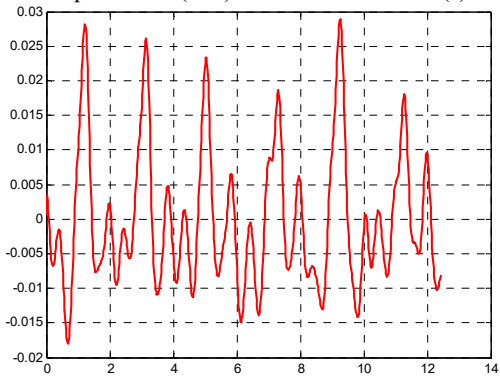
a) Pre-selected point number 17, displacement (mm) as a function of time (s)



b) Pre-selected point number 18, displacement (mm) as a function of time (s)



c) Pre-selected point number 19, displacement (mm) as a function of time (s)



d) Pre-selected point number 20, displacement (mm) as a function of time (s)

Fig. 4. Typical results of measurements of displacements of rollers at some of the measurement positions

5. Conclusions

Laser head “Microtrack LTC 200-100” was used in the performed investigation. Dynamic processes of rollers and of their segments were measured by using this laser head. The simplest method to make the rollers rotate in the process of experimental investigation is to rotate them manually. So, in the performed investigation this approach was adopted. Data of performed measurements were transferred to the personal computer. Planning the experimental investigation involved the pre-selection of a number of points in which measurements were performed. Low frequency filter was used in order to make the results of experimental investigations interpretable.

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Dynamical processes of complicated character are obtained as a result of performed measurements. The designed low pass digital filter after applying appropriate values of the parameters enables to obtain satisfactory correspondence with the results represented by the eigenmodes obtained numerically.

The results presented in the paper are used in the design of folding machines, which have various types of rollers in them. Also, these results obtained during investigations allow to determine the time when it is necessary to carry out the renewal of obsolete rollers in order that the folding of printing products would be qualitative.

Acknowledgements

The work was carried out on the basis of the Contract No. F5-90-1389.

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