

KAUNAS UNIVERSITY OF TECHNOLOGY FACULTY OF MATHEMATICS AND NATURAL SCIENCES

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MONTE CARLO MODELLING OF BRACHYTHERAPY SOURCE IN AN ANTHROPOMORPHIC HEAD PHANTOM

Final Master Degree Project

Supervisor:

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KAUNAS, 2017

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Final Master Degree Project Medical Physics (code 621B92002)

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KAUNAS, 2017

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ABBREVIATIONS

2D	Two Dimensional	
3D	Three Dimensional	
AAPM	American Association of Physicists in Medicine	
BREP	Boundary Representation (phantoms)	
CCS	Collapsed Cone Superposition	
СН	Condense History	
CLT	Central Limit Theorem	
СТ	Computed Tomography	
DICOM	Digital Imaging and Communications in Medicine	
DVH	Dose Volume Histogram	
GPU	Graphical Processor Unit	
GUI	Graphical User Interface	
HDR	High Dose Rate	
HPCC	High Performance Computing Center	
ICRU	International Commission on Radiation Units and Measurements	
ICRP	International Commission on Radiological Protection	
ICWG	Interstitial Collaborative Working Group	
ISA	Inter-Seed Attenuation	
LDR	Low Dose Rate	
MBCDA	Model Based Dosimetry Calculation Algorithm	
MC	Monte Carlo	
MOSFET	Metal–Oxide–Semiconductor Field-Effect Transistor	
MRI	Magnetic Resonance Imaging	
NCPTS	National Center of Physical and Technology Sciences	
PDF	Probability Distribution Function	
QA	Quality Assurance	
QMS	Quality Management Systems	
SPD	Solid Polymeric Dosimeter	
TLD	Thermoluminescence Dosimetry	
TPS	Treatment Planning System	

Ševčik, Aleksandras. Monte Carlo modelling of brachytherapy source in an anthropomorphic head phantom. Final Master Degree Project / supervisor prof. Diana Adlienė; Faculty of Mathematics and Natural Sciences, Kaunas University of Technology.

Research field and area: Biomedical Sciences, Medicine and Health.

Keywords: *Monte Carlo, simulation, brachytherapy, anthropomorphic head phantom* Kaunas, 2017. 74 p.

SUMMARY

Monte Carlo (MC) code was used to simulate the dose distribution during the head-related brachytherapy procedures. The simulation was performed with Fluka code and a voxel-based anthropomorphic head phantom taken from original Zubal Phantom which contains 25 anatomical regions with medium specified to be equivalent to the different tissues accordingly ICRU reports. The results show that heterogeneous tissues with different densities and compositions such as bone, an air in the mouth cavity and sinuses, and other created the fluctuations and influenced the dose absorption. It may be stated that in the cases where the source is placed or travel near the tissues of very different density such as bone or air-filled mouth cavity or sinus region, it may result in distortion of dose distribution and contribute to the higher overall uncertainty if compared with the doses obtained using standard treatment planning system. The results of performed simulations are expected to be used in the clinical practice for the analysis and verification of dose treatment plans in order to achieve more precise brachytherapy treatment and reduce the dose uncertainties.

Ševčik, Aleksandras. Brachiterapijos dozių pasiskirstymo vokseliniame žmogaus galvos fantome modeliavimas Monte Karlo metodu. Magistro baigiamasis projektas / vadovė prof. Diana Adlienė; Kauno technologijos universitetas, Gamtos ir matematikos mokslų fakultetas.

Mokslo kryptis ir sritis: Biomedicinos mokslai, Medicina ir sveikata.

Reikšminiai žodžiai: *Monte Karlo modeliavimas, simuliacija, brachiterapija, vokselinis, žmogaus galvos anatominis fantomas.*

Kaunas, 2017. 74 p.

SANTRAUKA

Šiame projekte buvo atlikta brachiterapinio šaltinio dozės pasiskirstymo galvoje simuliacija naudojant Monte Karlo metodą. Modeliavimas buvo atliekamas su Monte Karlo kodo programiniu paketu FLUKA ir Zubal VoxelMan antropomorfiniu vokseliniu galvos fantomu, kuris turi 25 skirtingus anatomines sritis su atitinkamai priskirtais anatominių audinių ekvivalentais. Simuliacijų rezultatuose parodyta heterogeninio skirtingų audinių tankio ir cheminės sudėties įtaka dozės pasiskirstymui ir pateiktos vizualios fliuktuacijos. Nustatyta, kad šaltiniui esant šalia ypač skirtingo tankio sričių, tokių kaip kaulai arba sinusų ančiai, realus dozės pasiskirstymas nėra tapatus dozės pasiskirstymui, skaičiuojamam pagal TG-43 protokolą, šaltiniui esant homogeniškoje vandens aplinkoje. Gauti rezultatai bus naudojami tolesnei analizei, siekiant tikslesnio dozės pasiskirstymo brachiterapijos procedūrose, taip pat panaudojami dozės verifikacijai esant sudėtingiems klinikiniams atvejams, pavyzdžiui, pacientui su žandikaulio metaliniu implantu ar kitais metaliniais artefaktais paciento burnoje.

1. INTRODUCTION

The main objective of radiotherapy is to deliver the lethal dose to target cells with minimum harm to the adjacent tissues. The main advantage of brachytherapy method is an ability to induce less harm to the surrounding areas while ensuring the high energy delivery to the malignant tissues due to Inverse Square Law property applied for the radiation field. In such case, it is essential to know the dose distribution of the source with the most available accuracy. It is recommended in TG43U1¹ that the initial dose distribution data should be obtained either by experiment or by Monte Carlo (MC) simulation using appropriate code to ensure the exact dose delivery to the patient.

Current clinical systems calculate the dose of brachytherapy source taking the medium as homogenous water equivalent. It may be expected that accuracy of dose rate and distribution may suffer due to the induced fluctuations in dose absorption of the actual heterogeneous tissues with different densities and compositions such as bone, an air in the mouth cavity and sinuses, or artificial implants as such. In extreme cases where the source is placed or travel near the media of very different density, it may result in different doses as compared to the water phantom based (standard) doses and result in the higher overall uncertainty than recommended.

This work aims to simulate the dose inhomogeneities during the head and neck patient brachytherapy treatment procedures occurring due to different tissues like bone, soft tissues, an air in the mouth cavity and sinuses, and other. The results will be used for further analysis in order to achieve more precise brachytherapy treatment and reduce the dose uncertainties in the clinical practice.

Dose distributions around brachytherapy source placed in a certain region of a voxel-based anthropomorphic head phantom adjusted from original Zubal Phantom^{2, 3} which contains 25 anatomical regions that are specified to be equivalent to the different tissues according to the ICRU reports^{4, 5}, have been modeled using MC simulation Fluka code^{6, 7}. The series of simulations have been performed analyzing the dose distribution and comparing it with water equivalent. The main goal of the performed modeling was to accurately simulate the dose distribution of brachytherapy source in 3D anthropomorphic human head phantom containing anatomic regions with corresponding tissue compositions and to assess the possibilities of the method with the aim of its using as a verification tool in Quality Assurance (QA).

The work also comprises brief presentation of the current mathematical formalism of the dose evaluation during brachytherapy treatment according AAPM TG-43 report⁸ and its updates¹ as well as the basics of MC method, mathematical formalism and the code used for the simulations.

2. LITERATURE OVERVIEW

2.1 Brief historical insight into the dosimetry of brachytherapy

The first procedures where radioactive nuclide was used for treatment of prostate cancer can be traced back to 1909⁹, however, only in 1982 the actual increase of the procedures can be noticed. The reason for this is that earlier was no technical means to ensure and guide the effective and safe usage of radioisotope. Improvements in radioactive source designs, introduction of new technical equipment and imaging methods enabled to make the brachytherapy as a conventional radiotherapy procedure in the oncology.

The development of practical cavity theory¹⁰ made a foundation for the technique to measure an exposure from radium sources. This system allowed to measure and calculates an exposure using ion chambers with sufficient wall thickness that enables charged-particle equilibrium. Later the achievements of computerized treatment planning and dosimetry methods in brachytherapy treatment planning enabled transfer from table-based systems to patient-specific 2D and 3D dose distributions. The NIST (the National Institutes of Standards and Technology) in the US announced the primary standards of reference exposure rate based upon carbon wall spherical ionization chambers for Cs-137 and Co-60 sources in 1974¹¹ and for Ir-192 brachytherapy sources in 1980¹². By the 1990 the thermoluminescence dosimetry (TLD) was accepted as the most reliable and best validated experimental dosimetry in brachytherapy, mostly due to the efforts of collaborative work of the institutional group known as Interstitial Collaborative Working Group (ICWG)¹³. This group prepared the reference procedures for calibrating TLD detectors and recommendations for correcting the higher TLD response to low-energy photons as well as coefficients to estimate the absolute dose rates in water quantitatively.

Advancements in radiobiology as well as new technological improvements contributed further to the development of brachytherapy. The reference dosimetry protocols have been developed⁸ by the joint collaboration of medical physicist teams under the lead of the American Association of Physicists in Medicine (AAPM). For the dosimetry of brachytherapy sources, the AAPM Task Group 43 (TG43) has established improved dose calculation formalism¹ that allowed. It consists of such factors as the dose rate constant, a radial dose function, an anisotropy function, a geometry factor, an anisotropy factor and the air kerma strength in respect with actual source construction and geometry in addition to the primary photon spectrum. As from the issue of this report, the number of research publications related to the dosimetry in brachytherapy has grown substantially, documenting both improved dosimetry methodologies and dosimetric characterization of used source models.

The new step was taken with development of MC code for radiation transport. The first

brachytherapy dose distributions computed by MC method were published by Meisberger in 1960s who calculated 1D tissue-attenuation and scatter build-up factors for point sources of the most common radionuclides¹⁴. Low-energy ¹²⁵I radionuclide was analyzed by Dale in 1983 who was the first one to use a Monte Carlo computational technique to establish the certain tables of parameters dosimetry of the brachytherapy nuclide in a variety of tissues and organs¹⁵ including the relation of the composition of a tissue with the dose absorbed at any location around the source. The commercial seed of the same ¹²⁵I radionuclide was simulated in 3D by Burns and Raeside¹⁶. The team modeled the seed submerged in a water phantom and calculated the dose rate per unit activity data expressed as a matrix surrounding the seed. Relative dose data were shown as 2D graph and compared with the reference data. Williamson's group in 1991 did the series of MC calculations of several radionuclides with high level of precision¹⁷. The experimental comparative measurements in water demonstrated that MC accurately reproduced the dose rates across the entire brachytherapy energy range in both homogeneous and heterogeneous phantom geometries¹⁸ which confirmed that MC simulations are adequately accurate to support clinical dosimetry.

The interest to brachytherapy treatment and the challenges of its dosimetry increased the number of MC-related brachytherapy peer-reviewed papers¹⁹ and recent simulations extend beyond the single source dosimetry with focus on patient-oriented applications.

2.2 Brachytherapy dose computation

The dose distribution around brachytherapy source depends on the emitted energy spectra, the geometry of the source and the surrounding material. The widely accepted dosimetry protocol, TG-43 report^{1, 8} has been established by the American Association of Physicists in Medicine (AAPM) which assumes a water medium with superposition of single source dose distributions, no inter-source attenuation (ISA) effects, and full scatter conditions at dose calculation points. Complex source geometry and a number of factors involved make manual dose calculations very tiresome, so computational treatment planning systems (TPS) are used. Precise operation of TPS in source localization and dose computations is absolutely necessary to ensure planned dose delivery.

The most treatment planning systems use mathematical formalism provided in TG-43 protocol¹ The TPS apply the source superposition method to cylindrically symmetric photon emitting brachytherapy source in the clinically defined volume. The software is able to visualize the distribution of isodoses and dose volume histograms (DVH) within the defined regions of source locations. It is to notice that the dose distributions planned by conventional brachytherapy TPS fit well when source shielding is negligible, the media of the volume of interest is equivalent to water over the used energy range and no high-Z materials are present. The low energy sources

are especially sensitive to these conditions but the high energy sources such as ¹⁹²Ir may be treated in the same way to some extent.

In the case of brachytherapy, MC is perfectly suited to solve the complex problem of particle transport and energy deposition within a heterogeneous medium such as tissues of the human body. An extensive evaluation of the MC method in radiotherapy is given by DeMarco²⁰, Seco and Verhaegen²¹ and references within.

The most established application of MC methods in brachytherapy is the determination of dose rate distributions around single radiation sources. While inverse square law dependence is the leading feature of brachytherapy dose distributions, photon attenuation and scatter build-up in the surrounding heterogeneous medium as well as particle interactions within the source assembly result in anisotropic dose distributions²². It is difficult to experimentally measure single-source dose distributions in brachytherapy due to the sharp dose gradients, low photon energies, and anisotropic dose rate curves. So the computational dosimetry techniques such as MC simulations became an crucial tool in brachytherapy²³. MC simulations allow a proper accounting for radiobiological effects in low-energy brachytherapy which involves calculation of photon and electron spectra at various distances from sources.

Modern techniques are being developed that includes MC simulations to the some extent. Full MC simulation is not clinically feasible at the moment. The big efforts have been made to develop the MC dose calculation algorithms used in the TPS²⁴. The main reason for this is a high computation power of multi-core computational systems that is required to gain viable simulations results. However MC codes are being utilized partly, merging pre-calculated Monte Carlo results and conventional TPS calculations and thus results obtained are usually more accurate than nonstochastic methods.

Several studies have compared MC dose calculations to the results of the TG-43 formalism analyzing different aspects of the dosimetrical quantities which are hard to measure experimentally, such as an impact of ISA²⁵, prostate implant geometries²⁶, tissue composition^{27, 28} founding the deviations of the dose to tissue up to 35% in certain cases.

As example of such merge of two methods the new treatment planning technique called Tufts technique was presented by Rivard et al^{29} in 2009 which may be applied in the clinical situations where the conventional approach is not adequate. Complex brachytherapy source configurations and their dose distributions from determined with Monte Carlo simulations were used as input data thus enabling new technique which uses conventional formalism adjusted with incorporated complex Monte Carlo-based brachytherapy dose distributions. In the result Rivard et al^{29} indicates that "[...] time needed to calculate dose was less than 1 s in all cases since the complex dose distribution for one virtual source was precalculated during the virtual source commissioning

phase and data were stored in the TPS", It is also stated that this fast calculation technique deviate less than 1% from full MC results. In addition, this technique also can be applied to calculate dose to a specific tissue type instead of dose to liquid water.

There is a high interest of developing MC-based treatment planning software, mainly utilizing the same principle of fast MC code adaption combined with biasing techniques to achieve clinically feasible computation times: TPSDose43³⁰, RayStretch³¹, egs_brachy³², gBMC³³ and others. One of the earliest programs, so called an accelerated Monte Carlo code MCPI³⁴ was presented in 2006 for dose calculation in prostate brachytherapy. MCPI models a set of low energy seeds with specific positions in a 3D heterogeneous phantom representing the prostate and surrounding tissue. It uses a phase space data and a hybrid geometry model for treatment of the interseed attenuation and tissue heterogeneity effects. It is reported that MCPI needs 59 s (single 2.4 GHz Pentium 4 CPU) to perform dosimetry.

BrachyDose is a general purpose Monte Carlo code for rapid brachytherapy calculations presented by Yegin et³⁵ al in 2006. The code uses the general EGSnrc code system³⁶ and is based on Yegin's MultiGeometry³⁷ auxiliary package. The tool may simulate high energy sources such as ¹⁹²Ir as well as full dose calculations from the seed implants for treatment planning where many seeds exist in the geometry, including inter-seed and tissue inhomogeneities effects. Dose is calculated by scoring collision kerma using a tracklength estimator and special biasing techniques are applied to reduce the computational time. The technique does not require disk space to store a phase space file. For typical low energy brachytherapy applications with ¹²⁵I seeds, only 510 s were used to calculate complete 3D dose distribution in a 1x1x1 mm3 array of voxels with a 2% statistical uncertainty. In other experiment, it took less than 30 seconds in (2 mm)³ voxels on a single 3.0 GHz core³⁸. Such results make it the program feasible in the clinical practice. In the benchmark with other methods, the calculations made with Brachydose show good agreement³⁹. Further development of the software include graphical user interface (GUI) and data integration in the DICOM-RT format while working towards clinical implementation^{38, 39}. Other researchers started to use it as well instead of original EGSnrc code⁴⁰.

Promising results were demonstrated with ALGEBRA⁴¹, a Monte Carlo platform for dosimetry in brachytherapy which is based on the GEANT4⁴² Monte Carlo code. It allows to place the source seeds in a realistic model of the patient made with appropriate chemical compositions and densities. Considering human tissues with different chemical compositions and densities different than water as well as interseed attenuation. the ALGEBRA is sufficiently fast and accurate for clinical and research purposes. ALGEBRA is developed as complete system fro brachytherapy dosimetry, that may use the DICOM RT formalism for image data handling and calculate the detailed dose distribution, consider the statistical uncertainties and create DVH for

the target. The calculation of the dose distribution takes around 12 min for a prostate case and in about 6 min for a breast case at 2% statistical uncertainty over a $2 \times 2 \times 2$ mm3 mesh. It also enables to compare MC calculations with TG43 or any other DICOM compatible dose calculation. Further developments include a user-friendly GUI and HDR dosimetry as well as an automatic seed optimisation. Dose distributions can be extracted for visualization with, e.g., BrachyGUI⁴³ which allows to generate three views of patient images with two sets of isodose lines, and the ratio map of two dose distributions, including dose, uncertainty, dose difference, gamma index, CT number, density, or material map display (**fig.1**).



Figure 1. BrachyGUI visual interface⁴³

However, by this day, despite being named as a reference dosimetry method for brachytherapy, MC has not been implemented in commercial TPS yet. In additional to TG-43 formalism, commercial TPS may use other methods as well, such as linear Boltzmann transport equation solver⁴⁴ and is implemented in Varian Medical Systems, Acuros^{TM45}. The newest version incorporated the option to calculate dose to voxel medium in the heterogeneous geometry using macroscopic kerma cross-sections to comply with TG186 recommendations⁴⁶.

Other methods of dose calculations in brachytherapy have been developed based on the collapsed cone superposition (CCS) algorithm. The collapsed cone algorithm is integrated to the Oncentra Brachy TPS from Elekta^{47, 48} and being updated to satisfy the new requirements of TG-186 protocol.

To summarize, currently most treatment planning systems use TG-43 protocol adaptations with specific computational approaches. However, this protocol has limited accuracy in certain cases as neglecting tissue heterogeneity, scattered radiation as well as applicator attenuation so implementation of new brachytherapy protocol TG-186 is under way into the clinical practice in which patient-specific phantom is used and heterogeneities are considered.

Papagiannis et al⁴⁹ states that both clinically available model-based dose calculation algorithms attain a dosimetric accuracy improvement compared with TG43-based calculations yet the clinical benefit from improved accuracy remains to be evaluated. As for MC based software, at the moment it remains more as verification tool in the quality assurance (QA) systems then the actually utilized treatment planning software.

2.3 Verification in brachytherapy as part of Quality Assurance

The new technologies and methodologies evolve rapidly together with increased demand to quality and safety of the patient treatment. The advancements in radiobiology and new understanding of level of uncertainties in low-level radiation and its possible part of inducing the secondary cancers all together with increased technological improvement requires new level of QA procedures. The patient-specific dose calculations are on focus now due to new advances in understanding of complex radiobiological damage phenomena^{50–52}.

The verification may be done at various levels, from simple manual calculation of every dose distribution to check if the TPS output is reasonable from to selective MC simulation of chosen patient dose calculation to see if optimal dose distribution is achieved. The first one is run as a step to prevent gross errors of human factor or system failure. With advancement in treatment technology using sophisticated dose optimization software, it has become a puzzling task to verify optimized dose delivery to prevent any gross errors in TPS output⁵³. The Nuclear Regulatory Commission states that a difference of 20% between the prescribed total dose and directed total dose to be a reportable medical event⁵⁴.

From a wider perspective the complex specifically chosen verification using MC simulation with included additional factors such as region boundary or different tissues may be seen as a part of continuous improvement in dose optimization protocols. The principle of continuous improvement is one of the core foundations of modern Quality Management Systems (QMS).

It is stated in Euratom Directive 2013/59 that "For all medical exposure of patients for

radiotherapeutic purposes, exposures of target volumes shall be individually planned and their delivery appropriately verified taking into account that doses to non-target volumes and tissues shall be as low as reasonably achievable and consistent with the intended radiotherapeutic purpose of the exposure"⁵⁵. This statement which is part of the optimization principle gives a basis for foundation of a patient-specific dosimetry. The new branches of radiotherapy emerge such as molecular radiotherapy^{56–58} with focus to indvidualize the dose to each person specifically according genetical and other factors.

It is mandatory for clinical applications that the dose distribution inside a patient should be evaluated and verified, which includes the non-point source configuration as well as attenuation and scattering of the radiation within the tissue. The dose distribution which is based only on the mathematical formulism are often limited. Actual brachytherapy sources are rarely spherical in structure and exhibit anisotropy due to self-attenuation of the radiation inside the source. Therefore the assumption that the radiation is isotopically produced around the source may lead to significant errors by neglecting the anisotropy of the source.

New technologies come to clinical practice such as real-time ultrasound guidance for brachytherapy, on-line imaging with ability to generate dose distribution delivered to the patient, real-time reoptimization of treatment plans with possibility of four-dimensional dose calculations to determine the actual dose delivered to tissue voxels. Combined with the principal need of optimization of radiation, a strong QA culture is essential. Verification of the dose delivered is an extremely important step in QA system which should become a daily routine in every institution. It also must be ensured that new systems are developed with verification methodology described as a part of the clinical implementation process. It may be firmly stated that in order to ensure the optimal treatment of patients, an institution must develop a suitable QA program for brachytherapy sources, equipment and the clinical procedures

The verification is an essential part of QA and has a requirement to be independent. Independent verification by two different protocols assures the quality of treatment. This should always be practiced to increase the accuracy of treatment even it's time consuming practice⁵⁹. The verification can be utilized by various means: using mathematical formulism, experimentally or using computational simulation software. Confirmation of the accuracy of optimized calculations with verification evaluation technique is vital in order to assure the accuracy of treatment⁵⁹.

2.4 Verification by mathematical formulism

Most of verifications proposed utilized some sort of mathematical formulism and are based on certain equations. The main purpose for such verification usually are protection from human errors

and miscalculations but it's rarely include other factors which was not included in pre-treatment dose calculation.

However in special cases there is a need for quick manual check of TPS output to avert systematic errors. In such cases the manual dose verifications may be used. This is especially true during commissioning after loading brachytherapy unit, where it is a requirement to include manual dose verification of TPS results⁵³. As an example, a quick mathematical method to verify the computational accuracy within 10% is given by Shanta⁵³:

$$D_{point} = \frac{S_K \cdot f_{(ak,wat)} \cdot WPF_{ri} \cdot t}{r^2}, \qquad (1)$$

where

 $S_{\rm k}$ – the source strength specified in air kerma strength,

WPF - the water perturbation factor (also referred to as Tissue Air Ratio),

r – the distance (in cm) from the center of the active source to the point of interest,

t – the duration of treatment,

f(ak,wat) – the air kerma to dose in water conversion factor.

As an additional example, the quick and easy independent verification check is proposed by Gadhi et al⁶⁰ to verify the output of TPS ABACUS 3.1 for the treatment of high dose rate intraluminal brachytherapy. The manual calculation deviates from the TPS result up to 2% only and may be used to enhance the reliability of brachytherapy treatment as a part of QA check to identify human error-related planning inaccuracies. The mathematical expression is simple and could be used for every procedure without use of much time. The author especially underlines that simplicity of technique claiming that no particular expertise is needed. The verification takes about one minute and does not significantly lengthen the patient's waiting time. It does not have an objective to optimize the prescribed dose but rather preventing the human or machine errors during periodic QA tests and serves as an independent safety layer.

There are many papers proposing the various techniques of manual mathematical verifications of TPS output during the brachytherapy procedures. They may be provided not only as mathematical formulas but may be developed based on workbooks/spreadsheets as well to simplify the verification itself and reduce its time. The more complex mathematical verification methods are proposed as software packages, but all of them mostly follow the TG-43 formalism and software package itself is for convenience and time-saving purposes^{61–63}.

2.5 Experimental verification

The other means of brachytherapy dose verification is an experimental way in which the actual dosimeters are used, usually a set of thermoluminescence dosimeters (TLD). A good example of it is a case study done by Nikoofar et al⁶⁴. The dosimeters were put in an anthropomorphic phantom constructed from natural bone and mixture of paraffin wax with sodium chloride. TLDs were placed in several depths in and around oesophagus. CT scans were used to avoid any discrepancy between the planned and the treated phantom set-up. In the paper it actually confirmed that dose distribution around sources not only was depended on distance from source and its size, but also was related to the tissues absorption and scattering. Several similar verification procedures using TLD are proposed^{65–68} including in-vivo TLD dosimetry^{69, 70}.

There is reported successful use of MOSFET dosimeter and diamond detector uses for the same purpose⁷¹. The dosimeter readings take at up to twelve locations on the surface in an anthropomorphic phantom. It also allows to place an array of dosimeters on the patient's skin verify the position in three-dimensions. In addition, the semiconductor properties allowed to automate process together with a mathematical algorithm which was made to evaluate the location of the source given a measured data set with contribution of tissue inhomogeneity. This study proposes the real-time system to verify brachytherapy procedure in vivo.

Other experimental methods include the use of radiochromic film⁷² and ionization chambers⁷³ as well as spectroscopic dosimetry^{74, 75}.

Chemical dosimetry takes a part of the methods that are used for dose measuring during the brachytherapy procedures. The polymer gel dosimeters have a real potential of the dose verification when complex irradiation regimes with multiple sources are involved in the specific geometry^{76–79}. Gel dosimeters are made from radiation sensitive material which polymerize as a function of the absorbed radiation dose. They have the capacity to image radiation dose distribution in 3D. Various accuracies are reported. Vandecasteele⁷⁶ reports that gel dosimetry allows to measure the absolute dose in the whole 3D volume within 5% accuracy. Comparison study by Senkesen et al⁸⁰ concludes that good agreement between the gel dosimetry and TPS results is achieved and may be used for HDR brachytherapy sources and 3D dose verification. In 2006 the solid polymeric dosimeter (SPD), was commercialized as PRESAGE⁷⁶. However, it must be noted that chemical dosimeters do not quantify the absorbed energy but rather count on expected relationship between the absorbed dose and the amount of the volumetric change of the dosimeter medium⁸¹. Therefore the main use of 3D dosimeters is the validation of the dose delivery and volumetric effect in comparison of the 3D dose distributions planned by the TPS.

2.6 Verification by MC simulation software

There are constant studies that note MC code as Quality Assurance QA tool⁸². The main general MC packages commonly used in the medical physics are MCNP, EGS4, EGSnrc, GEANT4, PENELOPE and FLUKA. The EGS4/EGSnrc codes especially very much used in the radiotherapy and dosimetry, representing a de facto standard for photon–electron transport in the energy range ($1 \div 10$ MeV) of radiotherapy interest⁸³.

MCNP⁸⁴ is a general-purpose Monte Carlo code that can be used for neutron, photon, and electron or coupled neutron/ photon/electron transport with very extended and powerful capabilities. A broad collection of cross-section data MCNP is developed and maintained at Los Alamos National Laboratory. Extremely wide applications almost in every case of the medical physics field is possible, including but not limited to any kind of shielding calculations, dose distributions, neutron and heavy particle interaction simulations, radio immunotherapy and boron neutron capture therapy, X-ray computed tomography and positron emission tomography simulations, many applications in nuclear medicine, etc. MCNP code is a leader used currently in such studies as dosimetry perturbations of the source within high-Z materials⁸⁵, dose distribution of difference media⁸⁶ or the update of treatment planning systems with more innovative dose calculation including patient-specific scatter and material heterogeneity conditions⁸⁷.

The Electron Gamma Shower (EGS4)⁸⁸ is a general purpose MC package able to simulate energies from a few keV up to several TeV. Originally developed at Stanford Linear Accelerator Center, USA for high energy physics applications, it has been extended to be applied for lower energy applications. EGSnrc^{36, 88} is an upgraded version of the EGS4 package. It is freely available for scientific community.

The GEANT⁴² was originally designed for high energy physics experiments in the CERN, but later was adjusted for the areas of medical and biological sciences, radiation protection and astronautics. The code may simulate electrons, positrons, γ -rays, X-rays, optical photons and muon interactions, as well as hadrons and ions interactions. However, it is toolkit, not the tool, and the extensive knowledge of the code as well as good C++ programming skills should be presented in order to use it successfully.

PENELOPE⁸⁹, Penetration and ENErgy LOss of Positrons and Electrons, is well known MC code mainly used for radiotherapy, dosimetry and nuclear medicine. It is capable of simulating all kinds of interactions (except nuclear) from 50 eV to 10⁹ eV. It is freely distributed for scientific purpose. PENELOPE uses a pure class II (mixed) algorithm for electrons/positrons which gives

the constancy under variation of simulation parameters.

FLUKA code is briefly presented in chapter 3.7.

The new MC codes are being developed currently such as GPU-based Monte Carlo dose calculation code DPM^{90, 91}, which allows to reduce the calculation time significantly, up to 5 to 7 times. However, there seems to be much more possibility in the using GPU architecture for MC calculations. As reported in the other research of GPU based MC code GPUMCD presented by Hissoiny et al⁹², GPUMCD is more than 900 times faster than EGSnrc in terms of simulation speed.

Being named as the most accurate simulation method MC is often used as a reference method to verify the dose distribution. The simulation gives the flexibility to include various parameters such as different media properties and complex geometries and is equivalent to the experiment itself due to the stochastic nature of the radiation itself. However, the method itself is subject to type A uncertainties in addition to type B and requires a lot of computational time which makes it clinically unfeasible. The various biasing options, however, enable to utilize MC simulation accuracy within reasonable times and provide the possibilities to use MC not only for verification but for treatment planning as well (see chapter 2.2 in this project for more details).

The question remains if analogue MC simulation may be still useful for dose calculation. While certainly not feasible in everyday clinical practise, it may have a benefit in case of complex cases such as patient with artificial jawbone where much of uncertainty is present. The unbiased analogue MC simulation yet takes a huge amount of time but allows to be used as "black box" with care. Analogue Monte Carlo samples for actual phase space distributions and gives a prediction of all statistical moments of any order and average quantities. In addition, it preserves correlations and reproduces fluctuations in the most accurate way.

Referring to this project, we see the potential of analogue unbiased MC simulation to be used as verification in the specific cases with complex geometry or high-Z materials are present. While specifically developed MC based software have limited flexibility, it is possible to utilize analogue MC simulations to get additional data for verification. Exemplary case of such event would be a patient with artificial jawbone having a head-neck cancer.

However, it should be pointed out that with improvements of GPU based MC codes the future of MC clinical use belongs to them due to unmatched efficiency and calculation speed.

2.7 Computational phantoms

Patient-oriented applications have an inherent need of anthropomorphic computational phantoms. From the phantoms based on simple quadratic equations in 1960s to voxelized phantoms based on actual medical images of the human body today is a major step that opens

many of new possibilities for the applications. Even the very first generation of MIRD phantom⁹³ gave the new insights for the dose calculation for individual organ (**fig. 2**).



Figure 2. The original MIRD phantom⁹⁴

Large degree of error and limited accuracy was an issue using such phantoms. The next generation could not come before the improved computer technology took the place. The actual breakthrough happened when computed tomography (CT) and magnetic resonance imaging (MRI) devices could create the accurate images of internal organs in 3D. This diagnostic data have been transformed into a voxel format enabling to reproduce the human body in digital form. More than 38 phantoms today are available worldwide for different uses⁹⁵.

Zubal and team at Yale University developed the VoxelMan phantom^{2, 3, 96} in 1994. The part of it is used in this project. The original phantom was created from head-to-torso and intended for improving nuclear medicine. Transmission computerized x-ray tomography (CT) was used to get the high resolution 3-dimensional human anatomy essential to construct the volume segmented phantom. Organ frameworks were manually drawn with millimetre resolution in each of 129 transverse slice images of the human torso (**fig. 3**). After the data has been set, the slices were transformed to get symmetric voxels of 4 mm, using a median compression scheme.



Figure 3. The slice of Zubal VoxelMan (taken from⁹⁷)

The third generation phantoms have become available, so called boundary representation phantoms which computational human models that contain anatomical structures of a human body using boundary representation method. Design of this type of phantom is realized by Non-Uniform Rational B-Spline method or polygonal mesh method, which are usually collectively called BREP methods⁹⁸. BREP phantoms are better suited for geometry deformation and adjustment in comparison to the voxel phantoms, and allow the morphing into an existing reference phantom or into the anatomy of a real patient for the calculation of individual-specific dose calculation (**fig.4**).



Figure 4. Three phantom generations: (a) Stylized phantom; (b) Voxel phantom (but displayed in smooth surfaces); (c) BREP phantom (taken from⁹⁹)

2.8 State of the art research in the 3D MC simulations of brachytherapy using voxelized phantoms and FLUKA

Patient-specific dose calculations is on focus today and MC simulations are anticipated to improve the current methodology using TG-43-style table-based source-superposition algorithms¹⁹. The effective utilization of MC simulations in a common clinical practice would allow including the effect of interseed attenuation (ISA) and tissue heterogeneities for low-energy seed and applicator shielding and boundary scattering effects for higher-energy brachytherapy routines.

Heterogeneity of the tissues and possible impact of the additional materials such as implants are on the focus now. When comes to anthropomorphic voxel phantoms, relevant for this project is the work of Abella and Miro where they calculated 3D dose distribution calculation in a voxelized human phantom for the external beam therapy¹⁰⁰ and especially the study of prostate brachytherapy using the similar phantoms by Furtado et al¹⁰¹. However, the results are presented as Dose Volume Histogram (DHV) and not directly comparable to our brachytherapy project.

Searches for the recent papers using FLUKA code with keyword for brachytherapy do not give many results. Just recently a feasibility study for beta-emitting brachytherapy source using FLUKA code was released by Anjomrouz et¹⁰² with positive evaluation. It can be seen that the code has mostly been dedicated to heavy ion therapy^{103–106}, radiation protection^{107–109} and particle physics^{110–112}. However, the recent improvements and future plans show that FLUKA intends to rise its popularity within the medical field beyond hadron therapy^{113–116}.

In general, the most of simulations are run for detail dosimetrical characteristics of sources in the various environments. The main code used for the simulations is MCNP while FLUKA is used rarely at the moment.We could not found comparative studies that would embrace the brachytherapy source inside the 3D voxelised anthropomorphic human phantom with assigned tissue equivalents and would show results in 3D.

2.9 Objective and tasks

All of above, the resulting objective is to use Monte Carlo (MC) package to accurately simulate the dose distribution of brachytherapy source placed in a certain position of 3D voxelised anthropomorphic human head phantom taking into account corresponding tissue compositions in the region of interest and evaluation of discrepancies between the dose values obtained from homogeneous media phantom and from modified heterogeneous media phantom calculations.

The objective will be achieved through the following tasks:

 Set-up and run the initial simulations of ¹⁹²Ir brachytherapy source in the water and air sphere for the check-up;

- 2) Modification of Zubal VoxelMan phantom^{2, 3, 96} and transformation of it into the FLUKAready geometry file;
- 3) Set-up and run the simulation of the source inside the tongue of the phantom when media of the regions are selected as water;
- 4) Set-up and run the simulation of the source inside the tongue of the phantom when media of the regions are selected as anatomically-equivalent;

3. MATERIALS AND METHODS

3.1 Background

A Monte Carlo simulation is based on repeated random sampling from probability

distributions representing the possible physical interactions applicable for the simulation. The independently simulated histories are summed up and post-processed to a numerical solution of the problem on the basis of the defined geometry, materials and the cross sections for the relevant interactions.

However, due to the complexity and required calculation time the method is not yet feasible for daily treatment planning in the clinics and typical TPS are using faster algorithms and derivations from MC for the daily basis. These systems are using certain assumptions such as unified material averaging the planning phantom geometry which is water in the most cases.

As it was stated above, there is a certain motivation to have the dose distribution as accurate as possible for the brachytherapy procedures. The human head consists of heterogeneous materials with different densities and compositions, and some areas such as mouth cavity or air-filled sinuses may be influencing dose distribution significantly.

This work simulates the dose distribution of Ir-192 source placed in the anthropomorphic head phantom region representing the middle of tongue. We intend to run the comparative simulations with (1) the phantom head consists of water only and (2) the phantom head consists of anatomically equivalent tissue compounds.

3.2 TG-43 formalism of dosimetry in brachytherapy

The dose distribution of a brachytherapy source is a complex function of the emitting energy spectra, the geometry of the source and the surrounding material. The widely accepted dosimetry protocol has been established by the AAPM TG-43 reports^{1, 8}.

The TG-43 formalism adopts a water medium with superposition of single source dose distributions, no ISA effects, and full scatter conditions (infinite or unbounded water medium) at dose calculation points.

The radial dose fall-off from any gamma source, the rate at which dose decreases with increasing distance from the source can be described by general 2D formalism given in the mentioned report:



r – distance (in cm) from the center of the active source to the point of interest,

 r_0 – denotes the reference distance which is specified to be 1 cm,

 θ – polar angle specifying the point of interest, P *r*, θ , relative to the source longitudinal axis, θ_0 – reference plane defines the source transverse plane, and is specified to 90°,

 $S_{\rm k}$ – source strength specified in air kerma strength,

 Λ – dose rate constant defined as the ratio of the dose rate at the reference point; the dose rate constant can be evaluated by using a calculation method such as the Monte Carlo method,

 $G_x(r,\theta)$ – geometry function that describes the effect of the active source material distribution within the source on the dose distribution outside the source,

 $g_x(r)$ – radial dose function accounting for the effects of absorption and scatter on the dose distribution in the medium along the transverse axis of the source,

 $F(r,\theta)$ – anisotropy factor describes the effects of anisotropic photon attenuation.

Calculation of the dose rate of encapsulated cylindrical source (**fig.5**), at point $P(r,\theta) = P(x,y)$ relative to the source center is shown in the figure below.



Figure 5. Coordinate system for brachytherapy dosimetry¹

The dose-rate constant in water, Λ , depends on both the radionuclide and source model. It is the ratio of dose rate at reference position $D(r_0, \theta_0)$, and S_K :

$$\Lambda = \frac{D(r_0, \theta_0)}{S_K},\tag{3}$$

where S_K represents air-kerma strength defined as the air-kerma rate $K_{\delta}(d)$ in vacuo at distance from the source center to the point of air-kerma specification:

$$S_K = K_\delta(d)d^2 \tag{4}$$

The geometry function is added to increase the accuracy with which dose rates can be projected by interpolation from data formulated at discrete points. It disregards scattering and attenuation, and is based on an effective inverse square-law correction using selected geometry model of the spatial distribution of radioactivity within the source. Two main models are recommended to be used for the geometry functions: point-source approximation and line-source approximation¹.

The radial dose function, $g_X(r)$, accounts for dose fall-off on the transverse-plane due to photon scattering and attenuation, and is defined by eq. 4:

$$g_X(r) = \frac{D(r,\theta_0)}{D(r_0,\theta_0)} \frac{G_X(r_0,\theta_0)}{G_X(r,\theta_0)}$$
(5)

The 2D anisotropy function describes the variation in dose as a function of polar angle relative to the transverse plane.

$$F(r,\theta) = \frac{D(r,\theta)}{D(r,\theta_0)} \frac{G_L(r,\theta_0)}{G_L(r,\theta)}$$
(6)

The complex 2D dose distribution is approximated then to 1D isotropic point-source equation:

$$D(r) = S_k \Lambda \frac{G_X(r, \theta r)}{G_X(r_0, \theta_0)} g_X(r) \cdot \phi_{an}(r)$$
(7)

The most treatment planning systems use the implementations of $eq.8^1$:

$$D(r) = S_k \Lambda \cdot \left(\frac{r_0}{r}\right)^2 g_p(r) \cdot \phi_{an}(r)$$
(8)

3.3 Basics of Monte Carlo simulation

MC techniques are broadly used in natural sciences, including medical physics. It may be defined as a numerical method to solve equations or to calculate integrals based on random number sampling¹⁹. In general, we may state that we want to use this method to solve the problem of particle transport.

The Monte Carlo simulation of a given experimental arrangement involves the numerical generation of random histories. To simulate these histories "interaction model" is needed, i.e., a set of differential cross sections for the relevant interaction mechanisms. These cross sections determine the probability distribution functions (PDF) of the random variables that describe a track;

- free path between successive interaction events,
- type of interaction taking place,
- energy loss and angular deflection in a particular event,
- initial state of emitted secondary particles, if any

Once these PDFs are known, random histories can be generated by using suitable sampling methods. If the number of generated histories is large enough, by the law of large numbers quantitative information on the transport process may be obtained by simply averaging over the simulated histories

The concept of phase space is used to describe the mathematics of particle transport¹¹⁹. A phase space of a dynamical system is a space in which all possible states of a system are represented, with each possible state corresponding to one unique point. Each phase space dimension corresponds to a particle degree of freedom. Generally three dimensions correspond to position in real space, another three dimensions represent the moment of the particle, the other dimensions is the particle type itself, evolution time, quantum numbers, etc. Each particle is represented by a point in a phase space, and the overall number of particles in an infinitesimal phase-space region can be expressed:

$$dN = f(x, p, t, \alpha)d^{3}pd^{3}xdtd^{n}\alpha$$
(8)

where f is a probability density function.

Particle transport is represented by the evolution of $f(x,p,t,\alpha)$ due to due to transport, scattering, particle absorption, decay, external forces, particle production, etc.¹²⁰. This evolution is described by Boltzmann's transport equation¹²¹. It is an equilibrium equation in phase space: at any phase space point, the increment of angular flux Ψ in an infinitesimal phase space volume is equal to sum of all entering particles minus sum of all leaving particles. If we name the initial particle distribution function in a given phase space region as source, while a phase space region where the modified $f(x,p,t,\alpha)$ is to be calculated is to be a detector, the solution can be written as:

$$f(x, p, t, \alpha) = \iiint G(x, p, \alpha, x', p', \alpha') f_0(x', p', \alpha') d^3 p' d^3 x' d^n \alpha'$$
(9)

where G s a multi-dimensional operator that includes all the microscopic processes.

It may be seen as the solution of any particle transport problem is a multi-dimensional integral in which all processes are described by probability distributions. The simplest solution can be written as an integral of $f(x,p,t,\alpha)$ over the region of interest:

$$N = \iiint_{\Delta p \Delta x \Delta \alpha} f(x, p, t, \alpha) d^3 p d^3 x d^n \alpha$$
(10)

The solution of the actual problem involving scattering, absorption, various interactions, etc. involves complex integrations in many variables and makes a numerical solution hardly achievable. Multidimensional numerical integration is required to solve the system of coupled transport equations for problems in radiation therapy, for example, for dose calculation, and

similar.

MC method can be seen as an integration method that allows Msolving multi-dimensional integrals by sampling from a suitable stochastic distribution. The main idea of MC simulation is to use random samples of parameters or inputs to analyze the behavior of a complex system or process. The mathematical foundation of this method is central limit theorem (CLT) which states the arithmetic mean of a sufficiently large number of iterates of independent random variables, each with finite expected value and finite variance, will be approximately normally distributed¹²². In other words, given any observable X, that can be expressed as the result of a convolution of random processes, the average value of X can be obtained by sampling many values of X according to the probability distributions of the random processes.

The accuracy of MC estimator depends on the number of samples:

$$\sigma \propto \frac{1}{\sqrt{N}} \tag{11}$$

Random sampling from probability distributions of the outcome of physical events is the base of MC integration ensured by use of pseudo-random numbers which are sequences that reproduce the uniform distribution generated from mathematical algorithms. Various sampling methods are used then to obtain the values.

Particle transport tens itself naturally to be simulated by Monte Carlo being a physical process described by probabilities (the particle cross sections are equal to the interaction probabilities per unit distance). It is a system of equations because the transport problem for photons, electrons and other particles must be solved. For the most cases of radiation therapy we are interested in electron (positron) and the photon transport including the interactions (bremsstrahlung, Compton scatter, photo electric absorption, pair production, etc.). Practically the parameter space is limited because the region of importance is limited the simulation is stopped if the photon or electron energy falls below some minimum energy.

Radiation transport through radioactive decay is a complex process which includes but is not limited to of attenuation and scattering of photons, carriage of beta rays and secondary electrons via elastic and inelastic collisions with orbital electrons including bremsstrahlung.

The whole particle history (**fig. 6**) is simulated including all secondary particles and its daughter particles.



Figure 6. Example of a particle history starting with a primary photon via Compton interactions and pair production events leading to secondary products¹⁹

The transport simulation of a particle discontinues if it leaves the geometry of interest or its energy falls below some predefined minimum energy o so called cut-off parameters. In the energy range of radiation therapy the processes of photoelectric absorption, Raleigh scatter, Compton scatter, and pair production are mostly relevant¹⁹. In every step through the simulation the certain values are calculated for accumulation, for example, the dose is calculated integrating the values of absorbed energy per voxel.

However, such even-by-event simulation is not suitable for charged particles like electrons or protons which undergo a very large number of single interactions. It means that the simulation of one electron history would require an unfeasibly long calculation time. The certain method is applied called Condense History (CH) technique which was introduced in 1963 by Berger¹²³. It is based on the assumption that almost all of charged particle interactions are elastic or semi elastic and only a tiny amount of energy is transferred from the charged particle to the surrounding matter on each interaction. In addition, the particle path angle changes in general only by small scattering angles and therefore it is possible to group many of these similar events into one CH step, where the direction change of the particle is simulated by one large multiple scattering angle¹²⁴. The most of MC algorithms perform electron, positron, proton, or heavier charged particle transport using the CH technique (**fig. 7**).



Figure 7. Example of a particle history starting with a primary electron (left side). In the right side the approximation of particle direction using the CH technique and path length corrections. Adapted from¹⁹

Photon interactions may also be simplified, for example, it is possible to model K-edge characteristic x-rays, but not consider L-edge x-rays for low-Z elements¹²⁵. Also it must be noted that radiological interactions at energies less than a few keV will be highly influenced by molecular binding effects, which are not accounted for in most current MC codes in use¹⁹.

Finally the suitable cross-section tables must be chosen and assigned to each material in the simulation geometry. The modern cross-section data are based on quantum mechanical models of each scattering and absorption process. The approximate models of orbital electron wave functions are used, with validation from available experimental measurements¹²⁶.

3.4 Geometry and material of the simulation

The TG-43 dose calculation formalism disregards patient tissue composition and is based upon specification of absorbed dose and transport of radiation in liquid water. The AAPM TG-43U1¹ report specifies liquid water to consist of exactly two parts hydrogen and one part oxygen with a mass density of 0.998 g/cm³ at a temperature of 22°C. However, it may be assumed that significant deviation between expected in delivered dose, especially for low-energy sources due to the patient tissue compositions, densities, and dimensions which differs from the reference geometry.

The linear attenuation coefficient μ is related to ρ , so the density differences between water and human tissues will result in different photon energy fluence and dose distributions. As μ/ρ is larger at low photon energies, alterations of elemental composition will result in higher dose differences for low-energy sources¹²⁷.



Figure 8. Linear attenuation coefficient for different absorbing mediums¹²⁸

The AAPM TG-186¹²⁹ is the systematic attempt to formulate guidelines for assigning cross sections and densities where it states that all-water approximation for dose calculations may considerably deviate at low (E < 50 keV) and intermediate (50 keV < E < 200 keV) and are critical for electronic sources where mean photon energies are generally about 30 keV.

The typical geometry used in the simulation of single-source brachytherapy dose distributions is a liquid water sphere of radius 15 cm for low energy sources¹ and 40 cm for higher energy sources¹³⁰. This represent doses in unbounded water medium over the clinically relevant distance range yet full scatter conditions are not met. It may be assumed that sources close to the skin will result in deviation of delivered dose²¹.

3.5¹⁹²Ir radionuclide in brachytherapy

Main characteristics of a radionuclide used in the brachytherapy can be described:

- By its half-life the time required for a quantity to reduce to half its initial value;
- By its specific activity decays per time unit per quantity of atoms;
- By its energy spectrum the energies that are emitted from the source.

Typical values of ¹⁹²Ir radionuclide used in the brachytherapy are given in the **table 1**.

The radionuclide is produced from enriched ¹⁹¹Ir targets (37% natural abundance) in a reactor by the (n, γ) reaction, creating¹⁹²Ir sources (typically 1 mm diameter by 3.5 mm length cylinders) with activities exceeding 4.4 TBq¹³⁰. HDR ¹⁹²Ir sources are encapsulated to ensure containment of the radioactive material and serve as a filter of unwanted radiation from beta rays produced through the source decay of 192 Ir (**fig.9**).



Table 1. Physical properties of Ir-192 radionuclide (adapted from¹³⁰)

Half-life	73.81 days
Type of disintegration	β^{-} (95.1%), EC (4.9%)
Maximum x-ray energy (keV)	78.6
Gamma energy-range (keV)	110.4-1378.2
Mean x-ray and gamma energy (keV)	350.0
Maximum β^- ray energies (keV)	81.7 (0.103%)
	258.7 (5.6%)
	538.8 (41.43%)
	675.1 (48.0%)
Mean β^- ray energy (keV)	180.7
Air-kerma rate constant,	0.1091
$\Gamma_{\delta = 10 \text{ keV}} (\mu \text{Gy m}^2 \text{ h}^{-1} \text{ MBq}^{-1})$	
Specific activity (GBq mg ⁻¹)	341.0

3.6 FLUKA code

Monte Carlo code FLUktuierende KAskade (FLUKA)^{6, 131} is a general-purpose tool for simulating the interaction of radiation with matter covering a wide range of applications from high-energy physics to medical and radiation physics, used by variety of organizations, including CERN and NASA^{131, 132}. The code is the standard tool used at CERN for dosimetry, radioprotection and beammachine interaction studies¹¹⁷.

FLUKA reads user input from an ASCII "standard input" file which contains a variable number of settings ("options"), each consisting of one or more lines ("cards"). The typical structure of a FLUKA input file is the following:

• Titles and comments for documentation purposes.

- Geometry. FLUKA uses constructive solid geometry (CSG) which allows creating a complex surface or objecting by using Boolean operators to combine simpler objects.
- Definition of the materials.
- Material assignments.
- Detectors. Each of these is a phase space domain (region of space, particle direction and energy) where the operator wants to calculate the estimates of a physical quantity such as fluence, etc.
- Biasing.
- Additional settings such as energy cut-offs, step size, physical effects not simulated by default, particles not to be transported, etc.
- Special commands involving magnetic fields, time-dependent calculations, writing of history files, transport of optical photons, event-by-event scoring, calling user-written routines, etc.
- Initialization of the random number sequence in order to get the estimation of statistical error.
- Starting signal and number of requested histories.

Fluka has a wide set of physics interactions available which are described by detail in the manual¹³³. As for our problem, it is important to know that Fluka allows semi-analogue mode of simulating radioactive decay. In this mode each single radioactive nucleus is treated in a Monte Carlo way like all other unstable particles: a random decay time, random daughters, random radiation are selected and tracked.

We'll run PRECISION physics set-up with activated detail transport of electrons, positrons and photons in addition to activated Rayleigh scattering and inelastic form factor corrections to Compton scattering and Compton profiles, detailed photoelectric edge treatment and fluorescence photons, multiple scattering, photon polarization taken into account for Compton, Rayleigh and photoelectric effects. Transport of charged particles is achieved through an original transport algorithm¹³⁴, including complete multiple Coulomb scattering treatment. At each transport step the fluctuations of energy of the discrete event and the continuous energy loss are taken into account. Accurate reproduction of average ionization and its fluctuations are performed due to a statistical approach alternative to the standard Landau and Vavilov¹³⁵

Photoelectric effect with accurate photoelectron angular distribution is based on the fully relativistic theory of Sauter¹³⁶. In addition, the photon polarisation is included for Compton, Rayleigh and photoelectric effects.

The lowest transport limit for electrons is 1 keV. The multiple scattering model becomes inaccurate below 20-30 keV in high Z materials, but optionally a single-scattering alternative may

be activated upon the request. It allows getting reasonable results in any material in the low energy range. As for photons, the lowest transport limit is 1 keV. But it must be noted that fluorescence emission may be misjudged at energies lower than the K-edge in high-Z materials, because of Coster-Kronig effect¹³³. The minimal recommended energy for primary photons is about 5 to 10 keV.

In this project we do not limit the production but we set transport cut. Due to practical reasons and associated problems of low-energy transport a particle transport threshold is set at 100 keV by the selected default options.

Typical input file is shown in the **fig.10** below.

TITLE						
Oras_Kapsule						
GLOBAL 100	0.0 0.0	0.0 0.0	1.0 0.	Cotting up global values and		
DEFAULTS			PRECISIO	Setting up global values and		
BEAM			ISOTOPE	beam properties. In our case, we		
BEAMPOS	0.0 0.0	0.0		choose an isotope source		
BEAMPOS	0.065	0.36	CYLI-VOL			
HI-PROPE 7	7. 192.					
GEOBEGIN			COMBNAME	Modelling the geometric		
0 0	MC-CAD			nrimitivos		
SPH ASphere1	0.00 0.00 0	0.00 98.00		printitives		
SPH ASphere2	0.00 0.00 0	0.00 103.00				
SPH ASphere3	0.00 0.00 0	0.00 200.00				
SPH extvoid 0.	00 0.00 0.0	0 1000.00				
SPH intvoid 0.0	0.0 0.00 0.0	0 500.00				
RCC shell1 0.0	0 0.00 -0.1	.8 0.00 0.00 0.4	5 0.09			
RCC shell2 0.0	0.0 0.27 0	.0 0.0 0.2 0.07				
SPH shell3 0.0	0 0.00 -0.1	.8 0.09				
RCC source 0.	00 0.00 -0.	17 0.00 0.00 0.3	6 0.065			
END						
BLACKHOL 5 +	-extvoid -i	ntvoid		Using boolean operators to		
VOID 5 +int	void -ASpł	nere3		establish the geometrical regions		
AIR2 5 +ASp	ohere3 -AS	phere2				
AIR3 5 +ASp	onerez -AS	pnere1				
AIR1 5 +ASp	onerel -sh	ell1 -shell2 -sh	ell3			
STEEL 5+she	ell1 -sourc	e +shell2 +sh	iell3 -source			
IRIDIUM 5+s	ource					
END						
GEOEND						
MATERIAL	77.	22.42	IRIDIUM	Material and compound		
MATERIAL 2	24.	7.18	CHROMIUM	description		
MATERIAL 2	25.	7.21	MANGANES			
MATERIAL 1	15.	1.82	PHOSPHO			
MATERIAL 1	16.	2.07	SULFUR			
* Steel316LN						
* Stainless steel	AISI316LN					
MATERIAL		7.8	SS316LN			
COMPOUND -	0.67145	IRON -0.185	CHROMIUM -0.1125	NICKELSS316LN		
COMPOUND -0.02 MANGANES -0.01 SILICON -0.00045 PHOSPHOSS316LN						
COMPOUND -	0.0003 S	ULFUR -0.0003	CARBON	SS316LN		
MATERIAL	78.	21.45	PLATINUM			
* lr192						
*						
MATERIAL 21.78 Ir192						
COMPOUND	-0.3 IRID	UM -0.7 PL	ATINUM Ir:	192		
MATERIAL	9. 0.	001696	FLUORINE			

* 104 Air dry (near sea level)				
*				
MATERIAL .00120484 AIR				
COMPOUND -1.248E-4 CARBON -0.755267 NITROGEN -0.231781	OXYGENAIR			
COMPOUND -0.012827 ARGON AIR				
ASSIGNMA BLCKHOLE BLACKHOL				
ASSIGNMA VACUUM void	Assigning the materials to the			
ASSIGNMA AIR AIR3	regions			
ASSIGNMA AIR AIR2				
ASSIGNMA AIR AIR1				
ASSIGNMA SS316LN STEEL				
ASSIGNMA Ir192 IRIDIUM				
RADDECAY 2.				
	Activating the decay physics for			
DCYSCORE -1. regdose dose USRBIN	the isotope source			
DCYSCORE -1. energ energ USRTRACK				
USRBIN 12. DOSE -30. AIR3 regdose				
USRBIN AIR3 &	Setting up the detectors			
USRBIN 11. DOSE -32. 200. 0.0 50.dose				
USRBIN 0.0 0.0 -50. 300. 1. 300. &				
USRTRACK -1. ENERGY -31. AIR3 500.energ				
USRTRACK 1E-2 1E-7 &				
SCORE ENERGY Initializing the random seed and				
RANDOMIZ 1.	setting up the number of histories			
START 1E8				
STOP				

Figure 10. The example of input file used for the (1) simulation

It should be stated that FLUKA has been developed to be a tool but not a toolkit. It is built and maintained with the most accurate physical models utilizing so called microscopic approach which gives the optimized performance at the single interaction level. Referring to Batisttoni¹³⁷, "[...] microscopic approach preserves correlations within interactions and among the shower components, and it provides predictions where no experimental data are directly available". There is a great potential of the use of FLUKA to medical applications, which in addition allows to translate DICOM files into voxel geometry as part of the Boolean geometry package of FLUKA¹³⁸.

3.7 Technical equipment

The MC simulation of complex geometries require a lot of computational power as billions of the events should be modelled typically to achieve the reasonable relative error. For such projects as the current one the cluster sites are need to gain results within the reasonable time frame.

For this project the services of High Performance Computing Center (HPCC) of the Lithuanian National Center of Physical and Technology Sciences (NCPTS) at Physics Faculty of Vilnius University ("HPC Saulėtekis")¹³⁹ has been used. The 128-core cluster site has been assigned for the needs of the simulations in this work which. The total amount of calculations time used for the all the simulations including the testing is estimated approx. 800 hr. As for the comparison, the job with the supercomputing facility took a little bit over 30 days when a typical desktop PC with 4-core pc will took more than 3 years of continuous run. This can be seen as

illustration of the computational needs for MC simulations.

The cluster consists of 16 calculation nodes. Each node has double Intel Xeon E5335 CPU resulting in 8-core computational power, 20-32GB RAM, 250GB 7.2K HDD. The nodes are connected through 1 Gbps network.

3.8 Evaluation of uncertainties

It is necessary to calculate the dose-rate constant accurately in order to obtain the absolute dose rates from the given air-kerma strength of the sources. Monte Carlo simulations can avoid such experimental uncertainties resulting from detector positioning and response artifacts and can yield artifact-free dose-rate estimates at the various distances¹. However, the accuracy of Monte Carlo is limited by the effects of geometric uncertainty, internal component movement, tolerances in the fabrication of sources, and small manufacturing changes on the uncertainty of calculated dose-rate distributions. In addition, it can be affected by inaccuracies in the geometric configuration of the source, uncertainties in the cross-sections and the modeling of the physical processes in the Monte Carlo code.

In general, the type B systematic uncertainty in MC simulations of radiation transport is influenced by used physics models, assumed transport assumptions, imperfect algorithms, input data uncertainty, the actual material composition, geometrical uncertainty, etc. In addition, there can be mistakes in the code or user mistakes such as mistyping the inputs, wrong normalization, etc. Type B uncertainties have not been systematically addressed in this work. A detailed discussion for their estimation and the difficulties associated with this question can be found in TG-43 associated reports presented in the first parts of the thesis. However, some remarks and notes are given for every simulation results if relevant.

Type A type uncertainty estimates are obtained as standard deviations of repeated measurement results. FLUKA code calculates the statistical error from for batches of several histories. The standard deviation of an estimator calculated from batches or from single histories is an estimate of the standard deviation of the actual distribution ("error of the mean" or "statistical error"). It is recommended to run at least 5-10 batches of comparable size¹³³. The MCNP guideline^{140–142} gives an insight of estimating the statistical error (**table 2**), which is confirmed as working with other codes¹³³. It must be noted, however, that it is empirically based on experience, not on a mathematical proof.

In this work we treat type A uncertainties with in-built tools in Flair tool and providing the statistical error value for every simulation in the results. Due to available technical resources we are able to keep it low.
Table 2. Estimation of relative error	or
---------------------------------------	----

Relative error	Quality of Tally
50 to 100%	Garbage
20 to 50%	Factor of a few
10 to 20 %	Questionable
< 10%	Reliable (except for detectors)
< 5%	Reliable

There are certain methodology requirements to be implemented into Monte Carlo modeling for testing and referencing the dose-rate estimates for the clinical use^{1, 130}. It must be stated, however, that the purpose of this thesis is not to provide a ready-to-use clinical reference but rather give insights on the possible heterogeneities due to different tissues, therefore not all the requirements are followed-up as they should not influence the overall result we are intend to achieve.

4. SIMULATIONS AND RESULTS

4.1 Introduction. Global parameters

We have used FLUKA version 2011.2c.5¹¹⁸ with following supporting software Flair¹⁴³ and SimpleGeo¹⁴⁴.

The modeled encapsulated source (**fig.11**) has an active core made of 192 Ir of effective density of 22.42 g/cm3 and active length of 3.6 mm. with active diameter of 0.65 mm. It is enclosed by the stainless steel AISI316LN encapsulation of density 7.8 g/cm3 with composition of iron, chromium, manganese, silicon, phosphorus, sulfur and carbon. The capsule is attached on a stainless steel cable with a diameter of 0.7 mm with length taken into the simulation not more than 2 mm.



Figure 11. The modelled geometry for encapsulated source

The following simulations were run:

- the encapsulated ¹⁹²Ir source in the 30 cm radius sphere when medium is the air and when the medium is the water for comparison purpose;
- (2) the non-encapsulated ¹⁹²Ir source (an active core only) in the water sphere of 30 cm radius versus the encapsulated source in the water sphere of the diameter for the comparison purpose;
- (3) the non-encapsulated ¹⁹²Ir source inserted in the tongue region of anthropomorphic human head phantom, two stages: a) with all regions equivalent to the water; b) with all regions modelled to the tissue-equivalent.

The exact input files of 1-3 models are listed accordingly in the appendices A-E.

4.2 Simulation I. The encapsulated source in the air and water sphere

The purpose of the simulation is to get an initial reference data and compare it with dose absorption in the water medium. In the first simulation the encapsulated source were placed in the 150 cm radius sphere with the medium equivalent to dry air, and after that the simulation we rerun with medium switched to the water. The simulation is run in 10 batches each with 10E9 histories reaching 10E10 histories in all. The radial dose rate decrease is shown in the graphs below per primary particle (**fig. 11-12**).



Figure 12. Z-X plane of dose distribution in the air sphere



In the graphs (**fig. 12-13**) the dose per decay is compared in the air and water mediums. The relative error is kept below 15% in the distance up to 30 cm. The graphs below are showing the dose distribution per decay in the relevant distances for the brachytherapy (radius up to 15 cm).



Figure 14. Dose per decay comparison in the air and water medium up to 20 cm from the active core center

The energy spectra graph was produced. As expected, the main energy range is 0.136-1.06 MeV range (**fig.15**). It is comparable with other works that report the similar energy spectra^{145, 146} (**fig. 16**).



Figure 15. ¹⁹²Ir energy spectrum obtained in this project



Figure 16. ¹⁹²Ir energy spectrum with comparison from other works: the results by Rodrigues et al¹⁴⁶ in the left graph and the results by Borg et al¹⁴⁵ in the right graph

4.3 Simulation II. The encapsulated compared with non-encapsulated source in the water sphere

It is not possible to directly combine the combinatorial geometry with voxel geometry while setting the modeling environment. As our main simulation will proceed in the voxelized human phantom, it means that we cannot model the encapsulated source inside. Instead the appropriate volume inside the phantom will be equalized to the size and parameters of the active core only. In such way it is meaningful to run the simple simulation to determine the possible differences between the dose distributions of encapsulated source versus active core only. The simulation was run in 10 batches with 10^8 histories each resulting in 10^9 histories and <5% relative error. The fig.17 below shows that there is no major difference in the dose per decay scoring in the water medium in both cases. It should be noted that the capsule absorbs the beta rays created through the source decay whiles photons are mostly not affected.



Figure 17. Comparison of encapsulated vs non-encapsulated source dose per decay

4.4 Simulation III. Dose distribution in anthropomorphic human head phantom

The used anthropomorphic human head model was adapted from Zubal phantom^{2, 3, 96} in which x-ray CT was used to create a computerized 3-dimensional 128x128x243 byte volume array modeling all major internal structures of the body of size . Each voxel of the volume contains an index number designating it as belonging to a given organ or internal structure (**fig.18**).



Figure 18. Sample image of Zubal head phantom⁹⁷

For this project we investigated the head part only to which 43 slices belong thus creating

128x128x43 active volume which consists of isotropic voxel dimensions of 4 mm.

Utilizing the special FORTRAN code we have converted the available phantom data to Fluka .vxl format which serves as an input for the simulation of the radiation transport using the voxel geometry (**fig.19**). The SimpleGeo¹⁴⁴ auxiliary software has been used to visualize it.



Figure 19. Zubal head phantom retransformed to the FLUKA .vxl format during the project. 3D shaded phantom is seen in the left side while the internal structure of the phantom with anatomical regions are shown in the right side

We simulated the dose distribution of 192 Ir source placed in the anthropomorphic head phantom region representing the middle of tongue. Two simulations were run. In the first simulation the medium of the all regions of the phantom were selected as water (i.e. *water phantom*). In the second simulation the anatomically-equivalent medium regions were created according the ICRU report and (i.e. *tissue phantom*). Each simulation was run in 100 batches containing of 10⁸ histories resulting in 10¹⁰ histories each thus enabling to keep the relative error below 5%.

The tissue composition was taken from literature reports, specifically by ICRU report No.46⁵, ICRP's phantom report⁹³ and work from Woodard and White¹⁴⁷. All the sources are indicated in the **table 3**.

In the following **figures 20-24** the inhomogeneity of *tissue phantom* in comparison with *water phantom* can be observed, especially in the air-filled sinus region. The fluctuations may be observed in the right picture representing the dose distribution in the *tissue phantom*. The **fig. 25** shows the uncertainty regions with corresponding values of relative error of the value for that bin.

Region	Organ corresponding the region	Media of the first simulation (<i>water</i> phantom)	Media of the second simulation (<i>tissue</i> phantom)
VOXEL02	skin	Water	Skin(ICRU)
VOXEL03	skeletal muscle	Water	Muscle skeletal (ICRU)
VOXEL04	jaw bone	Water	Bone, compact (ICRU)
VOXEL05	fat	Water	Adipose tissue (ICRU)
VOXEL06	pharynx	Water	Tissue, soft (ICRU)
VOXEL07	blood pool	Water	Blood (ICRU)
VOXEL08	bone marrow	Water	Skeleton-RedMarrow (Woodward, 1986)
VOXEL09	spine	Water	Bone, compact (ICRU)
VOXEL10	spinal cord	Water	Brain(ICRU)
VOXEL11	tongue	Water	Tissue, soft (ICRU)
VOXEL12	teeth	Water	Bone, compact (ICRU)
VOXEL13	spinal canal	Water	Water
VOXEL14	dens of axis	Water	Bone, compact (ICRU)
VOXEL15	hard palate	Water	Bone, compact (ICRU)
VOXEL16	skull	Water	Bone, compact (ICRU)
VOXEL17	sinuses/mouth cavity	Water	Air
VOXEL18	brain	Water	Brain(ICRU)
VOXEL19	medulla oblangata	Water	Brain(ICRU)
VOXEL20	cerebellum	Water	Brain(ICRU)
VOXEL21	cartilage	Water	Skeleton-Cartilage(Woodward, 1986)
VOXEL22	pons	Water	Brain(ICRU)
VOXEL23	eye	Water	Tissue, soft (ICRU)
VOXEL24	lens	Water	Eye lens(ICRU)
VOXEL25	optic nerve	Water	Brain(ICRU)
VOXEL26	cerebral falx	Water	Brain(ICRU)

Table 3. The media of the simulation phantoms



Figure 20. Dose distribution in water phantom (left) and tissue phantom (right). Transverse plane



Figure 21. Dose distribution in water phantom (left) and tissue phantom (right). Sagittal plane



Figure 22. Dose distribution in water phantom (left) and tissue phantom (right). Coronal plane



Figure 23. Dose distribution in water phantom (left) and tissue phantom (right). 3D model with dose limit to 1E⁻¹⁴ /

Bq.



Figure 244. The value of relative error for every bin for the water phantom simulation (A) and tissue phantom (B). Note significantly higher uncertainty in the latter. Pink threshold line shows the limit of 5% relative value

The summary **table 4** and the graph (**fig. 25**) is shown below illustrating the differences in dose distribution in the various regions.

			Dose in Gy per	Dose in Gy per	
Organ name	Tissue Appointed	Volume,	decay when	decay when tissue	Difference
		cm ²	region material	equivalent is selected	
skin	Skin(ICRII)	638 502	3 696F-15	3 4965-15	_5 71%
3811	Skin(ieito)	038.392	3.0901-19		-5.71%
skeletal muscle	Muscle skeletal (ICRU)	740.736	1.186E-14	1.161E-14	-2.21%
jaw bone	Bone, compact (ICRU)	75.712	2.334E-14	2.395E-14	2.52%
fat	Adipose tissue (ICRU)	31.936	7.405E-15	7.533E-15	1.70%
pharynx	Tissue, soft (ICRU)	10.56	2.236E-14	2.242E-14	0.25%
blood pool	Blood (ICRU)	15.232	6.039E-15	5.973E-15	-1.10%
bone marrow	Skeleton-RedMarrow (Woodward, 1986)	4.608	8.541E-15	8.467E-15	-0.87%
spine	Bone, compact (ICRU)	56.256	6.557E-15	6.915E-15	5.17%
spinal cord	Brain(ICRU)	9.152	5.069E-15	4.859E-15	-4.33%
tongue	Tissue, soft (ICRU)	37.632	1.109E-12	1.108E-12	-0.06%
teeth	Bone, compact (ICRU)	16.64	3.210E-14	3.309E-14	2.99%
spinal canal	Water	6.528	5.410E-15	5.035E-15	-7.44%
dens of axis	Bone, compact (ICRU)	0.96	1.035E-14	1.110E-14	6.77%
hard palate	Bone, compact (ICRU)	29.12	4.866E-14	4.890E-14	0.50%
skull	Bone, compact (ICRU)	519.296	3.580E-15	3.840E-15	6.76%
sinuses/mouth cavity	Air	82.368	1.852E-14	1.750E-14	-5.83%
brain	Brain(ICRU)	1171.136	2.862E-15	2.862E-15	0.03%
medulla oblangata	Brain(ICRU)	1.216	5.660E-15	5.327E-15	-6.24%
cerebellum	Brain(ICRU)	157.952	2.351E-15	2.190E-15	-7.38%
cartilage	Skeleton- Cartilage(Woodward, 1986)	53.76	9.228E-15	8.805E-15	-4.81%
pons	Brain(ICRU)	22.336	4.723E-15	4.716E-15	-0.16%
eye	Tissue, soft (ICRU)	15.488	7.675E-15	8.321E-15	7.76%
lens	Eye lens(ICRU)	1.472	6.105E-15	6.577E-15	7.18%
optic nerve	Brain(ICRU)	5.952	1.068E-14	1.075E-14	0.62%
cerebral falx	Brain(ICRU)	13.12	1.515E-15	1.582E-15	4.23%

Table 4. The summary table of the phantom simulations with $^{192}\mathrm{Ir}$



Figure 25. Differences in dose per decay between water and tissue phantom simulations with ¹⁹²Ir source

5. CONCLUSIONS

The simulation of the dose distribution of brachytherapy source within 3D voxelised anthropomorphic human head phantom has been performed taking into account corresponding tissue compositions. The discrepancies between the dose values obtained from homogeneous media phantom and from modified heterogeneous media phantom calculations were assessed.

- 1. The visualization of isodoses shows that actual dose distributions within appointed tissue equivalents differ from the clinically calculated distributions according TG-43 protocol when homogenous water medium is taken into calculations.
- 2. It is shown that the differences in the absorbed dose values between the water-built and tissue-built phantoms are up to 7.76 %. The dense material such as bone absorbed more energy and received higher dose then water-equivalent. The dose increase in the eye region could be result of the less energy absorption in the air-filled sinus region.
- 3. The data of the recognized Zubal phantom were translated to the format usable by FLUKA package. The translated phantom allows making the certain modifications in it thus giving an opportunity to use it in many other problems in the radiotherapy.
- 4. The project pioneered the methodic way in Lithuania of 3D tissue-based phantom use for Monte Carlo simulation of radiation transport for medical physicists. The tools used and described *know-how* can be easily re-used to solve any problem of such kind.

The project outcome confirms the impact of heterogeneous tissues to the dose distribution of brachytherapy source and enables to analyse the sensitivity of tissue composition on absorbed dose. It also may be used as the quality assurance tool for individual special-case patients such with certain implants near the source path to gain additional data next to the one provided by conventional treatment planning system.

6. ACKNOWLEDGEMENTS

I would first like to thank my thesis advisor prof. D. Adlienė of the faculty of Mathematics and Natural Sciences at Kaunas University of Technology who was always ready to help whenever I ran into a challenge or had a question about my research or writing and steered me in the right the direction whenever she thought I needed it.

I would also like to acknowledge the services of High Performance Computing Center (HPCC) of the Lithuanian National Center of Physical and Technology Sciences (NCPTS) at Physics Faculty of Vilnius University ("HPC Saulėtekis") which provided with technical basis to perform the simulations of this project.

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APPENDIX A

TTTI F						
GLOBAL	1000.0	0.0	0.0	0.0	1.0	0.
DEFAULTS						PRECISIO
BEAM						ISOTOPE
BEAMPOS	0.0	0.0	0.0			
BEAMPOS		0.065		0.36		CYLT-V0I
HT-PROPF	77.	192.		0.50		0.11 .01
GEOREGIN	,, ,	192.				COMBNAME
0 0		MC -	CAD			CONDINANE
* ASphara?		ne	CAD			
	0 00 0	00 0 00 15	Q			
* ovtvoid	0.00 0	.00 0.00 15	0.			
SDH avtvaid	0 00 0	00 0 00 10	00 00			
* intuoid	0.00 0	.00 0.00 10	00.00			
* Intvolu	0 00 0		0 00			
SPH INLVOID	0.00 0	.00 0.00 50	0.00			
* snelll		~ ~ ~ ~ ~	~~ ~ ~~			
RCC shell1	0.00 0	.00 -0.18 0	.00 0.00	0.45 0.09		
* shell2						
RCC shell2	0.0 0.0	0.27 0.0	0.0 0.2 0	.07		
* shell3						
SPH shell3	0.00 0	.00 -0.18 0	.09			
* source						
RCC source	0.00 0	.00 -0.17 0	.00 0.00	0.36 0.065		
END						
* Reg # 1						
* BLACKHOL; a	issigned i	naterial: B	lackhole;	mat # (1)		
BLACKHOL	5 +extvo	id -intvoi	d			
* Reg # 2						
<pre>* void; assig</pre>	gned mate	rial: Vacuu	m; mat #	(2)		
VOID	5 +intvo	id -Sphere				
* Reg # 4						
* AIR1; assig	gned mate	rial: Air;	mat # (29)		
SPHERE	5 +Sphere	e -shell1	-shell2	-shell3		
* Reg # 5						
* STEEL; assi	gned mate	erial: SS31	6LN; mat	# (27)		
STEEL	5 +shell:	1 -source	+shell2	+shell3	-source	
* Reg # 6						
* IRIDIUM; as	signed ma	aterial: IR	IDIUM; ma	t # (28)		
IRIDIUM	5 +source	2				
END						
GEOEND						
MATERIAL	77.		22.42			IRIDIUM
MATERIAL	24.		7.18			CHROMIUM
MATERTAL	25.		7.21			MANGANES
MATERIAL	15.		1.82			PHOSPHO
ΜΑΤΕΝΤΑΙ	16.		2.07			SUL FUR
* Steel316LN			2.07			JOLION
* Stainless	teel ATS	T316LN				
ΜΑΤΕΡΤΑΙ		191021	78			SS316LN
	0 67145	TRON	-0 185	CHROMTUM	-0 1125	NTCKELSS316LN
	-0 02	MANGANES	-0 01	STITCON	-0.00015	
	-0 0002		-0 0003		0.00045	CC3161 N
MATERTAL	0.0005 70	JULFUN	-0.0005 21 /F	CANDUN		
* Tp107	/0.		21,43			r la i linum
11 172 *						

MATERIAL			21.78			Ir192
COMPOUND	-0.3	IRIDIUM	-0.7	PLATINUM		Ir192
* 104 Air	dry (near s	ea level)				
*						
MATERIAL			.00120484			AIR
Compound	-1.248E-4	CARBON	-0.755267	NITROGEN	-0.231781	OXYGENAIR
Compound	-0.012827	ARGON				AIR
ASSIGNMA	BLCKHOLE	BLACKHOL				
ASSIGNMA	VACUUM	VOID				
ASSIGNMA	WATER	SPHERE				
ASSIGNMA	SS316LN	STEEL				
ASSIGNMA	Ir192	IRIDIUM				
RADDECAY	2.					
DCYSCORE	-1.			regdose	dose2	USRBIN
DCYSCORE	-1.			energ	energ	USRTRACK
USRBIN	10.	DOSE	-40.	150.	150.	150.regdose
USRBIN	-150.	-150.	-150.	300.	300.	300. &
USRBIN	11.	DOSE	-41.	150.	0.0	150.dose
USRBIN	0.0	0.0	-150.	600.	1.	600. &
USRBIN	11.	DOSE	-42.	150.	0.0	150.dose1
USRBIN	0.0	0.0	-150.	300.	1.	300. &
USRBIN	11.	DOSE	-43.	15.	0.0	15.dose2
USRBIN	0.0	0.0	-15.	300.	1.	300. &
USRTRACK	-1.	ENERGY	-60.	SPHERE		500.energ
USRTRACK	1E-2	1E-5				&
RANDOMIZ	1.					
START	1E9					
STOP						

APPENDIX B

TITLE						
GLOBAL	1000.0	0.0	0.0	0.0	1.0	0.
DEFAULTS						PRECISIO
BEAM						ISOTOPE
BEAMPOS	0.0	0.0	0.0			
BEAMPOS		0.065		0.36		CYLI-VOL
HI-PROPE	77.	192.				
GEOBEGIN						COMBNAME
0 0		М	C-CAD			
SPH Sphere	0.00 0	. 00 0.00	30.			
SPH extvoid	0.00 0	.00 0.00	1000.00			
SPH intvoid	0.00 0	.00 0.00	500.00			
RCC shell1	0.00 0	.00 -0.18	0.00 0.00	0.45 0.09		
RCC shell2	0.0 0.	0 0.27 0.0	0.0 0.2 0	0.07		
SPH shell3	0.00 0	.00 -0.18	0.09			
RCC source	0.00 0	.00 -0.17	0.00 0.00	0.36 0.06	5	
FND	0.000				-	
BI ACKHOI	5 +extvo	oid -intvo	bid			
VOTD	5 +intvo	id -Spher	re			
SPHERE	5 +Spher	e -shell'	- 1 -shell2	-shell3		
STEEL	5 +shell	1 -source	e +shell2	> +shell?	-source	
	5 +sourc			- 'Sherr	Jource	
	5 150010					
GEOEND						
MATERTAL	77		22 42			TRIDTIM
MATERIAL	24		7 18			
MATERIAL	24.		7.10			MANGANES
ΜΔΤΕΡΤΔΙ	2J. 15		1 82			PHOSPHO
MATERIAL	16		2.07			
* Stool3161	N 10.		2.07			SOLLON
* Stainless	stool ۵۲۵	T316LN				
ΜΔΤΕΡΤΔΙ	JUCCI AIJ	IJIOLN	78			SS316LN
	-0 67145		-0 185	CHROMTUM	-0 1125	
	-0 02	MANGANES	-0.01	STITCON	-0 00045	PHOSPHOSS316LN
	-0.02		-0 0003		0.00045	SS316LN
MATERIAL	78	JULI UN	21 45	CANDON		
MATERIAL	/0.		21.45			Tr192
	-03	TRTOTIM	-0.7			Ir 192 Tr192
MATERIAL	0.5	INIDION	00120484	TEATINON		
	-1 248F-4	CARBON	-0 755267	NTTROGEN	-0 231781	
	-0 012827		0.755207	NIMOGEN	0.251/01	ATR
* 276 Water	liquid H2					AIN
* Chemical	Formula	н 0	н			
MATERIAL	l'ol mara.	iii U	1.0			WATER
	2 0		1.0			WATER
			1.0	OXIGEN		WATER
	WATER	SDHERE				
	SS316LN	STEEL				
	55510EN Tn102					
	2	INIDION				
	2. _1			doco	doco	
	-⊥. 11		_ 10	uuse o	0050	
	лт. ТТ.	003E	-40. _1 F	200 7.	U.U 1	4.JUUSE 300 8
	U.U 1	10	-4.0	.00.	1.	500. d
START	1E0	10.				
STOP	TEA					
5101						

APPENDIX C

TITLE						
GLOBAL	1000.0	0.0	0.0	0.0	1.0	0.
DEFAULTS						PRECISIO
BEAM						ISOTOPE
BEAMPOS	0.0	0.0	0.0			
BEAMPOS		0.065		0.36		CYLI-VOL
HI-PROPE	77.	192.				
GEOBEGIN						COMBNAME
0 0		мо	C-CAD			
SPH Sphere	0.00 (a.oo a.oo a	30.			
SPH extvoid	0.00	9.00 0.00 1	1000.00			
SPH intvoid	0.00	9.00 0.00 5	500.00			
RCC source	0.00 (9.00 -0.17	0.00 0.00	0.36 0.06	5	
END						
BLACKHOL	5 +extvo	oid -intvo	oid			
VOID	5 +intvo	oid -Sphere	2			
WATER	5 +Sphei	re -source				
IRIDIUM	5 +sour	ce				
END						
GEOEND						
MATERIAL	78.		21.45			PLATINUM
MATERIAL			21.78			Ir192
COMPOUND	-0.3	IRIDIUM	-0.7	PLATINUM		Ir192
MATERIAL			.00120484			AIR
COMPOUND	-1.248E-4	CARBON	-0.755267	NITROGEN	-0.231781	OXYGENAIR
COMPOUND	-0.012827	ARGON				AIR
MATERIAL			1.0			WATER
COMPOUND	2.0	HYDROGEN	1.0	OXYGEN		WATER
MATERIAL	77.		22.42			IRIDIUM
ASSIGNMA	BLCKHOLE	BLACKHOL				
ASSIGNMA	VACUUM	VOID				
ASSIGNMA	WATER	WATER				
ASSIGNMA	Ir192	IRIDIUM				
RADDECAY	2.					
DCYSCORE	-1.			dose	dose	USRBIN
USRBIN	11.	DOSE	-41.	9.	0.0	4.5dose
USRBIN	0.0	0.0	-4.5	300.	1.	300. &
RANDOMIZ	1.	17484654.				
START	1E9					
STOP						

APPENDIX D

TITLE MasterWork GLOBAL 0.0 0.0 5000. 0.0 1. * Set the defaults for precision simulations DEFAULTS PRECISIO * Define the beam characteristics BEAM ISOTOPE HI-PROPE 77. 192. * Define the beam position BEAMPOS 24. 18. 3. 0.0 0.0 * Define the beam position BEAMPOS CYLI-VOL 0.0 0.065 0.35 GEOBEGIN COMBNAME VOXELS 0.0 0.0 0.0 target 0 0 * Black body SPH blkbody 0.0 0.0 0.0 1000. * Void sphere SPH void 0.0 0.0 0.0 500. END * Black hole BLKBODY 5 +blkbody -void * Void around VOTD 5 +void -VOXEL END GEOEND 15. PHOSPHO MATERIAL 1.82 2.07 SULFUR MATERIAL 16. MATERIAL 0.003214 CHLORINE 17. MATERIAL 19. 0.862 POTASSIU MATERIAL 30. 7.133 ZINC * Skin (ICRU) MATERIAL 1.1 SKTN COMPOUND -0.100588 HYDROGEN -0.22825 CARBON -0.04642 NITROGENSKIN COMPOUND -0.619002 OXYGEN -7E-05 SODIUM -6E-05 MAGNESIUSKIN PHOSPHO -0.00159 SULFUR -0.00267 CHLORINESKIN COMPOUND -0.00033 COMPOUND -0.00085 POTASSIU -0.00015 CALCIUM -1E-05 IRONSKIN COMPOUND -1E-05 ZINC SKIN * Muscle skeletal (ICRU) * MATERIAL SKELMUSC 1.04 COMPOUND -0.100637 HYDROGEN -0.10783 CARBON -0.02768 NITROGENSKELMUSC COMPOUND -0.754773 OXYGEN -0.00075 SODIUM -0.00019 MAGNESIUSKELMUSC COMPOUND -0.0018 PHOSPHO -0.00241 SULFUR -0.00079 CHLORINESKELMUSC -3E-05 -4E-05 COMPOUND -0.00302 POTASSIU CALCIUM IRONSKELMUSC COMPOUND -5E-05 ZINC SKELMUSC * 120 Bone, Compact (ICRU) MATERIAL 1.85 Bone Com -0.047234 HYDROGEN -0.14433 CARBON -0.04199 NITROGENBone Com COMPOUND PHOSPHOBone_Com COMPOUND -0.446096 OXYGEN -0.0022 MAGNESIU -0.10497 COMPOUND -0.00315 SULFUR -0.20993 CALCIUM Bone Com * 103 Adipose Tissue (ICRU) * from: ICRU Report #37, 1984, pub. by ICRU, Bethesda, Md, 20814, USA. MATERIAL 0.92 Adipose COMPOUND -0.119477 HYDROGEN -0.63724 CARBON -0.00797 NITROGENAdipose COMPOUND OXYGEN -0.0005 SODIUM -2E-05 MAGNESIUAdipose -0.232333 -0.00016 PHOSPHO -0.00119 CHLORINE COMPOUND Adipose * Tissue soft (ICRU) * MATERIAL 1.0 TISSUEIC COMPOUND -0.104472 HYDROGEN -0.23219 CARBON -0.02488 NITROGENTISSUEIC -0.00113 SODIUM -0.00013 MAGNESIUTISSUEIC COMPOUND -0.630238 OXYGEN -0.00133 PHOSPHO -0.00199 SULFUR -0.00134 CHLORINETISSUEIC COMPOUND -0.00199 POTASSIU -0.00023 CALCIUM -5E-05 COMPOUND IRONTISSUEIC COMPOUND -3E-05 ZINC TISSUEIC * Blood (ICRU) * MATERIAL 1.06 BLOOD -0.101866 HYDROGEN -0.10002 COMPOUND CARBON -0.02964 NITROGENBLOOD COMPOUND -0.759414 OXYGEN -0.00185 SODIUM -4E-05 MAGNESIUBLOOD COMPOUND -3E-05 SILICON -0.00035 PHOSPHO -0.00185 SULFURBLOOD COMPOUND -0.00278 CHLORINE -0.00163 POTASSIU -6E-05 CALCIUMBLOOD -0.00046 COMPOUND IRON -1E-05 ZINC BLOOD * Brain (ICRU) MATERIAL **RRATN** 1.03 COMPOUND -0.110667 HYDROGEN -0.12542 CARBON -0.01328 NITROGENBRAIN COMPOUND -0.737723 OXYGEN -0.00184 SODIUM -0.00015 MAGNESIUBRAIN -0.00354 PHOSPHO -0.00177 SULFUR -0.00236 CHLORINEBRAIN COMPOUND COMPOUND -0.0031 POTASSIU -9E-05 CALCIUM -5E-05 IRONBRAIN COMPOUND -1E-05 ZINC BRAIN * Skeleton-Red Marrow * from: Woodward & White, Brit. J. Radiology, vol. 59, 1216 (1986). MATERIAL 1.03 SkeleM COMPOUND -10.5 HYDROGEN -41.1 CARBON -3.4 NITROGENSkeleM -43.9 -0.2 SULFUR -0.2 CHLORINESkeleM COMPOUND OXYGEN COMPOUND -0.2 POTASSIU -0.1 IRON SkeleM * Skeleton-Cartilage * from: Woodward & White, Brit. J. Radiology, vol. 59, 1216 (1986). MATERIAL 1.1 Skeleton COMPOUND -9.6 HYDROGEN -9.9 CARBON -2.2 NITROGENSkeleton COMPOUND -74.4 OXYGEN -0.5 SODIUM -2.2 PHOSPHOSkeleton COMPOUND -0.9 SULFUR -0.3 CHLORINE Skeleton * Eye lens (ICRU) MATERIAL 1.1 EYE-LENS -0.099269 HYDROGEN -0.19371 COMPOUND CARBON -0.05327 NITROGENEYE-LENS COMPOUND -0.653751 OXYGEN EYE-LENS * ..+...1....+....2....+....3....+....4....+....5....+....6....+....7.. BLCKHOLE BLKBODY ASSIGNMA VACUUM VOID ASSIGNMA * Voxel cage VACUUM ASSIGNMA VOXEL * Air AIR VOXEL001 ASSIGNMA * Skin ASSIGNMA SKIN VOXEL002 * Skeletal muscle ASSIGNMA SKELMUSC VOXEL003 * Jaw bone ASSIGNMA Bone Com VOXEL004 * Fat ASSIGNMA Adipose_ VOXEL005 * Pharynx ASSIGNMA TISSUEIC VOXEL006
* Blood ASSIGNMA BLOOD VOXEL007 * Bone morrow SkeleM VOXEL008 ASSIGNMA * Spine ASSIGNMA Bone_Com VOXEL009 * Spinal cord ASSIGNMA BRAIN VOXEL010 * Tongue ASSIGNMA TISSUEIC VOXEL011 * Teeth ASSIGNMA Bone_Com VOXEL012 * Spinal canal ASSIGNMA WATER VOXEL013 * Dens of axis ASSIGNMA Bone_Com VOXEL014 * Hard palate ASSIGNMA Bone_Com VOXEL015 * Skull ASSIGNMA Bone_Com VOXEL016 * Sinuses/mouth cavity ASSIGNMA AIR VOXEL017 * Brain ASSIGNMA BRAIN VOXEL018 * Medulla oblangata BRAIN VOXEL019 ASSIGNMA * Cerebellum ASSIGNMA BRAIN VOXEL020 * Cartilage ASSIGNMA Skeleton VOXEL021 * Pons ASSIGNMA BRAIN VOXEL022 * Eye ASSIGNMA TISSUEIC VOXEL023 * Lens ASSIGNMA EYE-LENS VOXEL024 * Optic nerve ASSIGNMA BRAIN VOXEL025 * Cerebral falx BRAIN VOXEL026 ASSIGNMA RADDECAY 2. voxel26 DCYSCORE -1. Dose USRBIN USRBIN 10. DOSE -49. 40. 40. 20.Dose USRBIN 0.0 0.0 0.0 400. 400. 200. & 10. DOSE -50. 50. 20.Dose1 USRBIN 50. 0.0 0.0 200. & USRBIN 0.0 300. 300. USRBIN 12. DOSE -22. VOXEL002 voxel2 VOXEL002 & USRBIN 1. VOXEL003 USRBIN 12. DOSE -23. voxel3 VOXEL003 USRBIN 1. & USRBIN DOSE -24. VOXEL004 12. voxel4 USRBIN VOXEL004 1. & USRBIN 12. DOSE -25. VOXEL005 voxel5 USRBIN VOXEL005 1. & DOSE -26. VOXEL006 USRBIN 12. voxel6 VOXEL006 USRBIN 1. & USRBIN 12. DOSE -27. VOXEL007 voxel7 USRBIN VOXEL007 & 1. USRBIN DOSE -28. VOXEL008 12. voxel8 USRBIN VOXEL008 1. &

USRBIN	12.	DOSE	-29.	VOXEL009	voxel9
USRBIN	VOXEL009			1.	&
USRBIN	12.	DOSE	-30.	VOXEL010	voxel10
USRBIN	VOXEL010			1.	&
USRBIN	12.	DOSE	-31.	VOXEL011	voxel11
USRBIN	VOXEL011			1.	&
USRBIN	12.	DOSE	-32.	VOXEL012	voxel12
USRBIN	VOXEL012			1.	&
USRBIN	12.	DOSE	-33.	VOXEL013	voxel13
USRBIN	VOXEL013			1.	&
USRBIN	12.	DOSE	-34.	VOXEL014	voxel14
USRBIN	VOXEL014			1.	&
USRBIN	12.	DOSE	-35.	VOXEL015	voxel15
USRBIN	VOXEL015			1.	&
USRBIN	12.	DOSE	-36.	VOXEL016	voxel16
USRBIN	VOXEL016			1.	&
USRBIN	12.	DOSE	-37.	VOXEL017	voxel17
USRBIN	VOXEL017			1.	&
USRBIN	12.	DOSE	-38.	VOXEL018	voxel18
USRBIN	VOXEL018			1.	&
USRBIN	12.	DOSE	-39.	VOXEL019	voxel19
USRBIN	VOXEL019			1.	&
USRBIN	12.	DOSE	-40.	VOXEL020	voxel20
USRBIN	VOXEL020			1.	&
USRBIN	12.	DOSE	-41.	VOXEL021	voxel21
USRBIN	VOXEL021			1.	&
USRBIN	12.	DOSE	-42.	VOXEL022	voxel22
USRBIN	VOXEL022			1.	&
USRBIN	12.	DOSE	-43.	VOXEL023	voxel23
USRBIN	VOXEL023			1.	&
USRBIN	12.	DOSE	-44.	VOXEL024	voxel24
USRBIN	VOXEL024			1.	&
USRBIN	12.	DOSE	-45.	VOXEL002	voxel25
USRBIN	VOXEL025			1.	&
USRBIN	12.	DOSE	-46.	VOXEL026	voxel26
USRBIN	VOXEL026			1.	&
RANDOMIZ 1.324534635.					
* Set the number of primary histories to be simulated in the run					
START	1E8				

STOP